Results of Proficiency Test Fuel Oil December 2020

Organized by: Institute for Interlaboratory Studies

Spijkenisse, the Netherlands

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Report: iis20F03

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1 Introduction

Since 1994 the Institute for Interlaboratory Studies (iis) organizes a proficiency scheme for the analysis of Fuel Oil in accordance with the latest version of the specifications ISO8217 and ASTM D396 every year and twice per year since 2016. During the annual proficiency testing program 2020/2021 it was decided to continue the round robin for the analysis of Fuel Oil.

In this interlaboratory study registered for participation:

- 135 laboratories in 55 countries for Fuel Oil iis20F03
- 101 laboratories in 43 countries for Fuel Oil Metals iis20F03M
- 56 laboratories in 27 countries for Fuel Oil Bromine and p-Value iis20F03Br
- 58 laboratories in 30 countries for Fuel Oil Compatibility iis20F03C

In this interlaboratory study a total of 147 laboratories in 59 different countries registered for participation. See appendix 3 for the number of participants per country. In this report the results of the Fuel Oil proficiency tests are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT). Sample analyzes for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC17025 accredited laboratory. In this proficiency test the participants received, depending on the registration, from one up to four different samples of Fuel Oil, see table below.

Samples	Purpose
#20250 1x 1L	Regular analyzes
#20251 1x 100mL	Metal analyzes
#20252 1x 1L	Bromine number & p-Value
#20253 2x 40mL	Compatibility rating

Table 1: Fuel Oil samples used in PT iis20F03

Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). These PTs falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

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2.2 PROTOCOL

The protocol followed in the organization of these proficiency tests was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website site www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

For the preparation of the sample for regular analyzes on Fuel Oil a batch of approximately 200 liters was obtained from a third party. After heating to 60°C and homogenization 200 amber glass bottles of 1 liter were filled and labelled #20250.

The homogeneity of the subsamples was checked by determination of Density at 15°C in accordance with ISO12185 on 8 stratified randomly selected subsamples.

	Density at 15°C in kg/m³
Sample #20250-1	1007.8
Sample #20250-2	1007.8
Sample #20250-3	1007.8
Sample #20250-4	1007.8
Sample #20250-5	1007.8
Sample #20250-6	1007.8
Sample #20250-7	1007.8
Sample #20250-8	1007.8

Table 2: homogeneity test results of subsamples #20250

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Density at 15°C in kg/m³
r (observed)	0.00
reference test method	ISO12185:96
0.3 x R (reference test method)	0.45

Table 3: evaluation of the repeatability of subsamples #20250

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The calculated repeatability is in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the preparation of the sample for the Metal analyzes in Fuel Oil a batch of approximately 40 liters of Fuel Oil which contains metals was obtained from a third party. After heating to 60°C and homogenization 151 PE bottles of 0.1 liters were filled and labelled #20251. The homogeneity of the subsamples was checked by determination of Vanadium in accordance with IP501 on 8 stratified randomly selected subsamples.

	Vanadium in mg/kg
Sample #20251-1	90
Sample #20251-2	87
Sample #20251-3	93
Sample #20251-4	96
Sample #20251-5	92
Sample #20251-6	93
Sample #20251-7	93
Sample #20251-8	93

Table 4: homogeneity test results of subsamples #20251

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Vanadium in mg/kg
r (observed)	7
reference test method	IP470:05
0.3 x R (reference test method)	9

Table 5: evaluation of the repeatability of subsamples #20251

The calculated repeatability is in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the preparation of the sample for the Bromine and p-Value in Fuel Oil Determination in Fuel Oil a batch of approximately 130 liters of Fuel Oil was obtained from a third party. After heating to 60°C and homogenization 80 amber glass bottles of 1 liter were filled and labelled #20252.

The homogeneity of the subsamples was checked by determination of Density at 15°C in accordance with ISO12185 on 8 stratified randomly selected subsamples.

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	Density at 15°C in kg/m³
Sample #20252-1	1008.0
Sample #20252-2	1007.9
Sample #20252-3	1007.9
Sample #20252-4	1007.9
Sample #20252-5	1007.9
Sample #20252-6	1007.9
Sample #20252-7	1007.9
Sample #20252-8	1007.9

Table 6: homogeneity test results of subsamples #20252

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Density at 15°C in kg/m³
r (observed)	0.10
reference test method	ISO12185:96
0.3 x R (reference test method)	0.45

Table 7: evaluation of the repeatability of subsamples #20252

The calculated repeatability is in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

For the preparation of the sample for the Compatibility Determination two different batches of Fuel Oil, which were not compatible, of approximately 3.5 liters each were obtained from a third party. After heating to 60°C and homogenization 80 amber glass vials of 40mL were filled and respectively labelled A and B. One subsample A and one subsample B were put together in a plastic bag and the bag was labelled #20253. The homogeneity of subsamples A or B were checked by determination of Density at 15°C in accordance with ISO12185 on respectively 8 stratified randomly selected subsamples.

	Sample A - Density at 15°C in kg/m³	Sample B - Density at 15°C in kg/m³	
Sample #20253-1	981.8	893.1	
Sample #20253-2	981.8	893.2	
Sample #20253-3	981.7	893.2	
Sample #20253-4	981.8	893.1	
Sample #20253-5	981.7	893.1	
Sample #20253-6	981.6	893.1	
Sample #20253-7	981.7	893.1	
Sample #20253-8	981.6	893.1	

Table 8: homogeneity test results of subsamples #20253

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From the above test results the repeatabilities were calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

	Sample A - Density at 15°C in kg/m³	Sample B - Density at 15°C in kg/m³	
r (observed)	0.23	0.13	
reference test method	ISO12185:96	ISO12185:96	
0.3 x R (reference test method)	0.45	0.45	

Table 9: evaluation of the repeatabilities of subsamples #20253

The calculated repeatabilities are in agreement with 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

Depending on the registration of the participant the appropriate set of PT samples was sent on November 25, 2020. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The stability of Fuel Oil packed in the amber glass and PE bottles was checked. The material was found to be sufficiently stable for the period of the proficiency test.

2.6 ANALYZES

The participants were requested to determine on sample #20250: Total Acid Number, API Gravity, Ash Content, Asphaltenes, Calculated Carbon Aromaticity Index (CCAI), Carbon Residue micro method, Conradson Carbon Residue, Density at 15°C, Flash Point PMcc, Heat of Combustion (Gross and Net), Kinematic Viscosity (at 50°C and 100°C), Viscosity Stabinger (at 50°C and 100°C), Nitrogen, Pour Point (Lower, Upper and Automated), Sediment by Extraction, Total Sediment (Existent, Accelerated and Potential), Total Sulfur, Water by distillation, Water and Sediment, Vacuum Distillation at 10 mmHg but reported as AET (IBP, 5% - 50% recovered and FBP) and Total Carbon, Total Hydrogen and Total Nitrogen (CHN Analyzer). Also, some extra information was requested about the determination of Total Acid Number.

On sample #20251 it was requested to determine Aluminum as Al, Silicon as Si, Sum of Aluminum and Silicon, Iron as Fe, Nickel as Ni, Sodium as Na, Vanadium as V, Calcium as Ca, Phosphorus as P and Zinc as Zn.

On sample #20252 Bromine Number and p-Value and on sample #20253 it was requested to report the Compatibility rating after blending of the two samples.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

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To get comparable test results a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods (when applicable) that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyzes). Additional or corrected test results are used for data analysis and the original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care.

The assigned value is determined by consensus based on the test results of the group of participants after rejection of the statistical outliers and/or suspect data.

According to ISO13528 all (original received or corrected) results per determination were submitted to outlier tests. In the iis procedure for proficiency tests, outliers are detected prior to calculation of the mean, standard deviation and reproducibility. For small data sets, Dixon (up to 20 test results) or Grubbs (up to 40 test results) outlier tests can be used. For larger data sets (above 20 test results) Rosner's outlier test can be used. Outliers are marked by

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D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations. For each assigned value, the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1, was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve (dotted line) was projected over the Kernel Density Graph (smooth line) for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. EN, ISO or ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent on the variation in this interlaboratory study.

This target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used, like Horwitz or an estimated reproducibility based on former iis proficiency tests

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

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The z-scores were calculated according to:

```
z_{\text{(target)}} = \text{(test result - average of PT)} / \text{target standard deviation}
```

The $z_{(target)}$ scores are listed in the result tables of appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

```
|z| < 1 good
1 < |z| < 2 satisfactory
2 < |z| < 3 questionable
3 < |z| unsatisfactory
```

4 **EVALUATION**

Some problems were encountered with the dispatch of the samples due to COVID-19 pandemic. Therefore, the reporting time on the data entry portal was extended with another two weeks.

For the PT on regular analyzes in Fuel Oil: four participants reported test results after the extended final reporting date and fifteen participants did not report any test results at all. For the PT on Metals analyzes in Fuel Oil: two participants reported test results after the extended final reporting date and fifteen participants did not report any test results at all. For the PT on Bromine Number and p-Value in Fuel Oil determination: one participant reported the test results after the extended final reporting date and fourteen participants did not report any test results at all.

For the PT Fuel Oil Compatibility rating: three participants reported the test results after the extended final reporting date and eleven participants did not report any test results at all.

Finally, over the four PTs 129 participants reported in total 2778 numerical test results. Observed were 81 statistically outlying test results, which is 2.9%.

In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

Not all data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

4.1 EVALUATION PER SAMPLE AND PER TEST

In this section the reported test results are discussed per sample and per test. The test methods which were used by the various laboratories were taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the original data. The abbreviations, used in these tables, are explained in appendix 4.

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In the iis PT reports ASTM test methods are referred to with a number (e.g. D473) and an added designation for the year that the test method was adopted or revised (e.g. D473:07e1). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D473:07e1(2017)). In the test results tables of appendix 1 only the test method number and year of adoption or revision (e.g. D473:07e1) will be used.

Sample #20250

procedure A.

Total Acid Number: This determination was very problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers was not at all-in agreement with the requirements of ASTM D664:18e2 procedure A. Therefore, no z-scores were calculated. Even when the test results of only IP or only BEP were evaluated separately the calculated reproducibilities after rejection of the statistical outlier were not in agreement with the corresponding requirements of ASTM D664:18e2

ASTM D664 was updated in 2018. One of the major changes is the buffer used for in the end point detection (pH11 is changed to pH10). The solubility of Fuel Oil in the solvent mentioned in ASTM D664 can be poor. Regular cleaning of the electrodes as described in the method is recommended to obtain reliable and consistent test results.

API Gravity: This determination was not problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical

outliers is in agreement with the requirements of ASTM D1298:12b(2017).

Ash Content: This determination was very problematic at an ash content of 0.030%M/M.

Four statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not at all in agreement with the

requirements of ISO6245:01 and ASTM D482:19.

Asphaltenes: This determination was not problematic. One statistical outlier was

observed. The calculated reproducibility after rejection of the statistical outlier is in full agreement with the requirements of IP143:04. ASTM

D6560:19 is equivalent to IP143.

<u>Calculated Carbon Aromaticity Index:</u> This determination was not problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO8217:17.

<u>Carbon Residue micro method:</u> This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO10370:14.

<u>Conradson Carbon Residue:</u> This determination was not problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D189:06(2019).

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- <u>Density at 15°C:</u> This determination was not problematic. Five statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO12185:96.
- <u>Flash Point PMcc:</u> This determination was not problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of ISO2719-B:16.
- Heat of Combustion (Gross): This determination was problematic for a number of participants. Four statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D240:19.
- Heat of Combustion (Net): This determination was problematic for a number of participants. Four statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D240:19.
- <u>Kinematic Viscosity at 50°C:</u> This determination was not problematic. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO3104:20.
- <u>Kinematic Viscosity at 100°C:</u> This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO3104:20.
- <u>Viscosity Stabinger at 50°C:</u> This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D7042:16e3.
- <u>Viscosity Stabinger at 100°C:</u> This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D7042:16e3.
- Nitrogen: This determination was problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D5762:18a.
- <u>Pour Point Lower:</u> This determination was not problematic. Two statistical outliers were observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ISO3016:19.
- <u>Pour Point Upper:</u> This determination was not problematic. Two statistical outliers were observed and two other test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ISO3016:19.

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- <u>Pour Point Automated:</u> This determination was problematic. No statistical outliers were observed. The calculated reproducibility is not in agreement with the requirements of ASTM D5950:14(2020).
- <u>Total Sediment by Extraction:</u> This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D473:07e1(2017).
- <u>Total Sediment Existent (TSE):</u> This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of IP375:11(2018).
- Total Sediment Accelerated (TSA): This determination was not problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP390:11(2017). IP390:11 is identical to ISO10307-2:09 and technically equivalent to ASTM D4870:18.
- Total Sediment Potential (TSP): This determination was not problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP390:11(2017). IP390:11 is identical to ISO10307-2:09 and technically equivalent to ASTM D4870:18.
- Total Sulfur: This determination was problematic depending on the test method used. Four statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO8754:03 but not with the stricter requirements of ASTM D4294:16e1.
- <u>Water by distillation:</u> This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO3733:99 or ASTM D95:13(2018).
- <u>Water and Sediment:</u> This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D1796:11(2016).
- Vacuum Distillation at 10 mmHg but reported as AET: This determination was not problematic for all parameters except for 10% recovered. In total eight statistical outliers were observed and four other test results were excluded. All calculated reproducibilities after rejection of the suspect data are in agreement with the requirements of ASTM D1160:18, except the calculated reproducibility for 10% recovered.

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CHN-Analyzer:

This determination was not problematic for Total Carbon and Total Hydrogen but was problematic for Total Nitrogen. In total three statistical outliers were observed.

The calculated reproducibilities for Total Carbon and Total Hydrogen after rejection of the statistical outlier are in agreement with the requirements of ASTM D5291-ABC:16. The calculated reproducibility for Nitrogen after rejection of the statistical outliers is not in agreement with the requirements of ASTM D5291-ABC:16.

Sample #20251

Aluminum:

This determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with the requirements of IP470:05 and IP501:05.

Silicon:

This determination was problematic depending on the test method used. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

Sum Aluminum and Silicon: This determination was problematic depending on the test method used. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

This determination was problematic depending on the test method used. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier in agreement with the requirements of IP470:05 and IP501:05.

> This determination was problematic depending on the test method used. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of IP470:05 and IP501:05.

This determination was problematic depending on the test method used. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

Iron:

Nickel:

Sodium:

Calcium:

Vanadium:

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<u>Phosphorus:</u> This determination was not problematic. The reporting participants agreed

on a value near or below the application range. Therefore, no z-scores are

calculated.

<u>Zinc:</u> This determination was problematic depending on the test method used.

Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP470:05 but not in agreement with the stricter requirements of IP501:05.

Finally, it should be noted that proper attention for homogenization is crucial for a material such as Fuel Oil. Due to the nature of the material it is very susceptible to problems when not handled correctly. Practically every test method for the determination of metals in Fuel Oil has similar statements regarding homogenization. It is recommended to use a quality control fuel oil with known amounts of metals like Al, Fe, Si and V. This control standard may be of use to detect deviations in metals with respect to the preparation steps.

Sample #20252

Bromine: This determination was problematic. Three statistical outliers were

observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D1159:07

(2017).

<u>p-Value:</u> This determination was not problematic. No statistical outliers were

observed. The calculated reproducibility is in agreement with the

requirements of SMS1600.

Sample #20253

<u>Compatibility:</u> This determination was problematic. Two statistical outliers were observed.

The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D4740-M:20). No effect was observed between the type of reference used for spot determination.

4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from literature reference test methods (in casu ASTM, EN, ISO and IP test methods) are presented in the next tables.

Parameter	unit	n	average	2.8 * sd	R(lit)
Total Acid Number	mg KOH/g	60	0.11	0.10	(0.02)
API Gravity		68	8.8	0.2	0.5
Ash Content	%M/M	86	0.030	0.012	0.005
Asphaltenes	%M/M	61	8.18	1.68	1.64
Calc. Carbon Aromaticity Index		69	862.9	1.6	2.2
Carbon Residue micro method	%M/M	79	15.78	0.99	1.54

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Parameter	unit	n	average	2.8 * sd	R(lit)
Conradson Carbon Residue	%M/M	29	15.94	1.40	2.51
Density at 15°C	kg/m³	101	1008.1	1.3	1.5
Flash Point PMcc	°C	105	100.2	5.8	6
Heat of Combustion (Gross)	MJ/kg	53	41.91	0.40	0.40
Heat of Combustion (Net)	MJ/kg	42	39.66	0.35	0.40
Kinematic Viscosity at 50°C	mm²/s	92	716.1	37.5	60.6
Kinematic Viscosity at 100°C	mm²/s	75	48.34	2.50	5.83
Viscosity Stabinger at 50°C	mm²/s	17	714.3	37.6	73.5
Viscosity Stabinger at 100°C	mm²/s	16	47.92	0.79	3.44
Nitrogen	mg/kg	38	3782	1171	1006
Pour Point, Lower	°C	40	4.8	8.0	9
Pour Point, Upper	°C	71	6.9	8.3	9
Pour Point Automated, Δ3°C	°C	29	3.3	12.3	6.1
Total Sediment by Extraction	%M/M	67	0.017	0.023	0.037
Total Sediment Existent (TSE)	%M/M	65	0.015	0.018	0.036
Total Sediment Accel. (TSA)	%M/M	59	0.017	0.018	0.038
Total Sediment Potential (TSP)	%M/M	60	0.016	0.018	0.037
Total Sulfur	%M/M	104	3.39	0.25	0.29
Water by distillation	%V/V	73	0.05	0.06	0.2
Water and Sediment	%V/V	39	0.05	0.07	0.11
Initial Boiling Point	°C	30	192.8	31.9	49
5% recovered	°C	30	277.9	26.5	26.9
10% recovered	°C	31	326.7	24.8	21.7
20% recovered	°C	30	397.0	16.2	19.8
30% recovered	°C	30	453.0	13.8	17.7
40% recovered	°C	30	493.6	12.6	15.6
50% recovered	°C	20	523.3	8.2	14.5
Final Boiling Point	°C	30	524.1	21.4	27
Total Carbon	%M/M	24	85.4	1.8	2.4
Total Hydrogen	%M/M	22	10.2	0.6	0.7
Total Nitrogen	%M/M	18	0.43	0.19	0.10

Table 10: reproducibilities of tests on sample #20250

Element	unit	n	average	2.8 * sd	R(lit)
Aluminum as Al	mg/kg	75	5.1	3.0	2.3
Silicon as Si	mg/kg	69	6.4	5.3	4.8
Sum of Aluminum and Silicon	mg/kg	62	11.7	5.8	5.4
Iron as Fe	mg/kg	78	17.4	6.4	10.5
Nickel as Ni	mg/kg	81	34.3	12.3	16.3
Sodium as Na	mg/kg	79	11.5	5.8	5.7

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Element	unit	n	average	2.8 * sd	R(lit)
Vanadium as V	mg/kg	85	95.6	.6 22.8 31.	
Calcium as Ca	mg/kg	67	4.5	2.7	4.1
Phosphorus as P	mg/kg	63	<1	n.e.	n.e.
Zinc as Zn	mg/kg	54	0.99	0.60	0.58

Table 11: reproducibilities of tests on sample #20251

Parameter	unit	n	average	2.8 * sd	R(lit)
Bromine Number	g Br ₂ /100g	34	14.5	5.4	4.7
p-Value		30	1.30	0.24	0.6
Compatibility		45	3.7	2.2	1

Table 12: reproducibilities of tests on sample #20252 and #20253

Without further statistical calculations it can be concluded that for a number of tests there is a good compliance of the group of participants with the reference test method. The problematic tests have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF DECEMBER 2020 WITH PREVIOUS PTS

	December 2020	June 2020	December 2019	June 2019	December 2018
Number of reporting laboratories	129	153	137	147	134
Number of test results	2778	2810	2945	2713	2948
Number of statistical outliers	81	89	115	86	92
Percentage of statistical outliers	2.9%	3.2%	3.9%	3.2%	3.1%

Table 13: comparison with previous proficiency tests

In proficiency test, outlier percentages of 3% - 7.5% are quite normal

The performance of the determinations of the proficiency tests was compared against the requirements of the reference test methods. The conclusions are given in the following table.

Parameter	December 2020	June 2020	December 2019	June 2019	December 2018
Total Acid Number	()	()	()	()	+
API Gravity	++	+	++	+	++
Ash Content					-
Asphaltenes	+/-		()	-	-
Calc. Carbon Aromaticity Index	+	+	+	+	+
Carbon Residue micro method	++	+	+	+	+
Conradson Carbon Residue	+	+	+/-	+/-	+
Density at 15°C	+	-	+	-	+
Flash Point PMcc	+/-	-	+	+/-	+/-
Heat of Combustion (Gross)	+/-	+/-	+	+	+

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Parameter	December 2020	June 2020	December 2019	June 2019	December 2018
Heat of Combustion (Net)	+	+/-	+/-	+	+
Kinematic Viscosity at 50°C	+	+	-	+	+/-
Kinematic Viscosity at 100°C	++	+	+	+/-	+
Viscosity Stabinger at 50°C	++	++	+	++	+
Viscosity Stabinger at 100°C	++	++	++	++	+
Nitrogen	-	-	-	+/-	-
Pour Point Lower	+	-	+	-	-
Pour Point Upper	+/-	+	+	-	-
Pour Point Automated, Δ3°C		+	+/-	-	-
Total Sediment by Extraction	+	+	+	+	++
Total Sediment Existent (TSE)	++	++	++	++	++
Total Sediment Accel. (TSA)	++	++	++	++	++
Total Sediment Potential (TSP)	++	++	++	++	++
Total Sulfur	+	+	+	+	+/-
Water by distillation	++	++	++	++	++
Water and Sediment	+	+	+	++	+
Distillation at 10 mmHg to AET	+	-	+/-	-	+
Total Carbon	+	+	+	+	+
Total Hydrogen	+	+	+	+	+
Total Nitrogen	-		+	-	-
Aluminum as Al	-	-	+/-	+/-	+/-
Silicon as Si	-	-	+	+	+/-
Sum of Aluminum and Silicon	+/-	-	+/-	+/-	+/-
Iron as Fe	+	+	+	+	++
Nickel as Ni	+	+	++	++	++
Sodium as Na	+/-	+/-	+	+	+
Vanadium as V	+	+	+	+	+
Calcium as Ca	+	-	-	-	+/-
Phosphorus as P	n.e.	+	+	+/-	+
Zinc as Zn	+/-	-	+/-	+/-	+
Bromine Number	-	+	n.e.	+	n.e.
p-Value	++		n.e.	++	n.e.
Compatibility		-	n.e.	-	n.e.

Table 14: comparison determinations against the reference test methods NB.No -z-scores were calculated for the evaluations between brackets

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The following performance categories were used:

++ : group performed much better than the reference test method

+ : group performed better than the reference test method

+/- : group performance equals the reference test method

- : group performed worse than the reference test method

-- : group performed much worse than the reference test method

n.e. : not evaluated

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APPENDIX 1

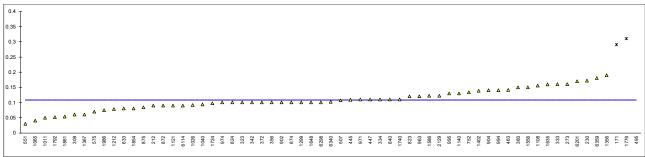
Determination of Total Acid Number on sample #20250; results in mg KOH/g

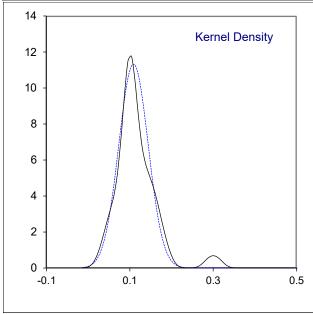
Deteill	ililation of	Total Acid Nullibel	UII Saiii	ipie #20	200, 10	Sulto III I	ing itom	9		
lab	method	value	mark	z(targ)	lab	method		value	mark	z(targ)
52	D664-A	<0.10			904	D664-A		0.14		
120	D664-A	<0.1			913	200171				
	D004-A									
140					914					
150	D664-B	<0.10			962					
154					963	D664-A		0.12		
159					971	D664-A		0.11		
168					974	D664-A		0.10		
169					994	D664-A		0.14		
170					995	D664-A		0.13		
171	D664-A	0.29	R(0.01)		996					
175					997					
212	D664-A	0.09			1011	D664-A		0.05		
225	200.71				1016	200.71				
	Dec4 A					Dec4 A				
230	D664-A	0.1723			1026	D664-A		0.0914		
237					1040	D664-A		0.0935		
238					1065	D664-A		0.0399		
253					1108	D664-A		0.156		
256					1109	D664-B		< 0.01		
273	D664-A	0.16			1121	D664-A		0.09		
						D004-A				
309	D664-A	0.06			1126					
311	D664-A	<0.10			1134					
313					1140	IP177		0.13		
323	D664-A	0.10			1167					
333	D664-A	0.16			1205					
334	D664-A	0.11			1212	D664-A		0.078		
	D004-74									
336					1213	D664-A		<0.1		
339					1277					
342	D664-A	0.10			1299	D664-A		0.10		
349					1320					
351					1356	D664-A		0.19		
356	D664-A	0.10			1367	IP177		0.06		
			<u></u>			11 177				
360	D664-A	0.150	С		1381					
370					1397					
372	D664-A	0.10			1402	IP177		0.138		
381					1510					
445	D664-A	0.109			1556	D664-A		0.15		
447	D664-A	0.11			1585					
463	D664-A	0.141				D664-A		0.122		
			D(0.04)		1586	D004-A				
495	D664-A	2.083	R(0.01)		1631					
507	D664-A	0.107			1635	D664-A		0.159		
541					1648	D664-A		0.10		
551	D664-A	0.03			1650					
558					1681					
575	D664-A	0.07			1720					
	D004-A	0.07				DCC4 D				
610					1724	D664-B		0.097		
621					1740	D664-A		0.11		
631					1776	D664-A		0.31	R(0.01)	
633	D664-A	80.0			1792	D664-A		0.052	•	
634					1796					
657	D664-A	<0.10			1854	D664-A		0.08		
						D004-M				
704	D664-A	< 0.1			1857	D004 4		0.054		
732					1881	D664-A		0.054		
752	D664-A	0.1335			1906					
753					1949					
778					1986	D664-A		0.075	С	
781	D664-A	<0.1			2129	IP177		0.122	•	
	D004-74					11 177				
785					6054					
798					6075					
823	D664-A	0.12			6092					
824	D664-A	0.1			6112					
825					6114	D664-A		0.090		
840	D664-A	0.11			6201	D664-A		0.030		
						D004-M				
872	D664-A	0.09			6238					
873	D664-A	less 0.1			6262					
874	D664-A	0.10			6298	D664-A		0.10		
875	D664-A	0.084			6340		D664-A	0.102		
887					6359		D664-A	0.180		
902	D664-A	0.10					200+71	5.100		
302	D004-1∕	0.10			İ					

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		Only IP	Only BEP
normality	OK	OK	OK
n	60	36	9
outliers	3	1	0
mean (n)	0.1084	0.1099	0.1065
st.dev. (n)	0.03518	0.02830	0.03042
R(calc.)	0.0985	0.0792	0.0852
st.dev.(D664-A:18e2 IP 125 mL)	(0.00770)	(0.00781)	
R(D664-A:18e2 IP 125 mL)	(0.0216)	(0.0219)	
compare			
R(D664-A:18e2 IP 60 mL)	(0.0651)	(0.0658)	
R(D664-A:18e2 BEP 125 mL)	(0.0306)		(0.0300)
R(D664-A:18e2 BEP 60 mL)	(0.0634)		(0.0623)

Lab 360: first reported 0.205 Lab 1986: first reported 0.0075





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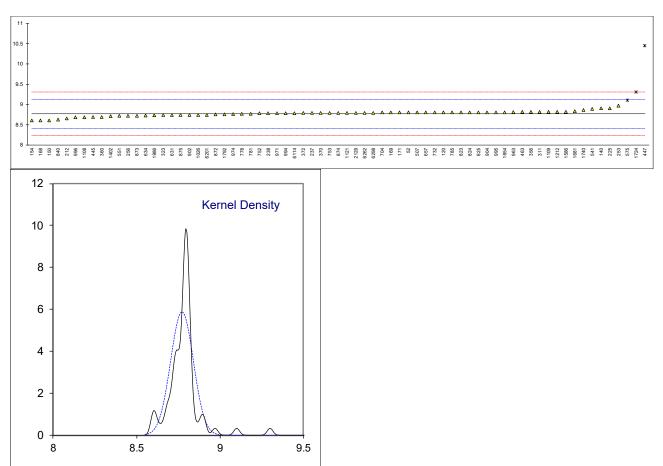
Determination of API Gravity on sample #20250

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4052	8.8		0.16	904	D1298	8.8		0.16
120	D4052	8.8		0.16	913	B 1200			
140	D4052	8.9		0.72	914				
150	D287	8.6		-0.96	962				
154	D4052	8.6		-0.96	963	D1298	8.81		0.22
159					971	D1298	8.78		0.05
168	D287	8.6		-0.96	974	D1298	8.76		-0.06
169	D1298	8.8		0.16	994	D1250	8.78		0.05
170	2.200				995	D1250	8.8	С	0.16
171	D4052	8.8		0.16	996	D1298	8.68	J	-0.51
	D4032					D1290			
175	10040405				997				
212	ISO12185	8.65		-0.68	1011				
225	D4052	8.9		0.72	1016				
230					1026	D4052	8.74		-0.18
237	D4052	8.79		0.10	1040				
238	D1298	8.78		0.05	1065				
253	D4052	8.97		1.11	1108	ISO12185	8.68		-0.51
256	D1298	8.72		-0.29	1109	D287	8.82		0.27
273	D 1230			-0.23	1121	D4052	8.79		0.10
					1121	D4032	0.79		0.10
309	D.1000								
311	D1298	8.82		0.27	1134				
313					1140				
323	D1298	8.74		-0.18	1167				
333					1205				
334					1212	ISO12185	8.82		0.27
336					1213				
339					1277				
342					1299				
349					1320				
351					1356				
356	D4052	8.82		0.27	1367				
360	D4052	8.69		-0.46	1381				
370	ISO12185	8.79		0.10	1397				
372	D1298	8.79		0.10	1402	D4052	8.71		-0.34
381					1510				
445	IP365	8.69		-0.46	1556				
447	D1250	10.45	R(0.01)	9.40	1585				
463	D1298	8.82		0.27	1586	D1298	8.82		0.27
495					1631				
507	D1298	8.80		0.16	1635				
541	D4052	8.89		0.66	1648				
551	D4052	8.72		-0.29	1650				
558	2.002				1681	ISO12185	8.83		0.33
575	D1298	9.1	C,R(0.01)	1.84	1720	10012100			
610	D1290		O,11(0.01)	1.04	1724	D1298	9.3	D(0.01)	2.96
								R(0.01)	
621	D.4050	0.74		0.40	1740	D4052	8.863		0.51
631	D4052	8.74		-0.18	1776	10040405	0.75		0.40
633	D.1000				1792	ISO12185	8.75		-0.12
634	D1298	8.7249		-0.26	1796	D 4050			
657	ISO12185	8.80		0.16	1854	D4052	8.8		0.16
704	D1298	8.80		0.16	1857				
732	D1250	8.80		0.16	1881				
752	D1250	8.78		0.05	1906				
753	ISO12185	8.79		0.10	1949				
778	D1298	8.77		-0.01	1986	D1298	8.73		-0.23
781	ISO12185	8.77		-0.01	2129	D1298	8.79		0.10
785	D1298	8.8		0.16	6054	·= • •			
798	B 1200				6075				
823	ISO12185	8.8		0.16	6092		_		
824	ISO12185	8.8		0.16	6112	D4050	0.70		0.05
825	D1298	8.8		0.16	6114	D4052	8.78		0.05
840	ISO12185	8.62		-0.85	6201	D4052	8.74		-0.18
872	D1298	8.75		-0.12	6238				
873	D1298	8.72		-0.29	6262	D4052	8.79		0.10
874	D1298	8.79		0.10	6298	D4052	8.79		0.10
875	D1250	8.74		-0.18	6340				
887					6359				
902	D1298	8.74		-0.18					
					•				

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normality	suspect
n	68
outliers	3
mean (n)	8.772
st.dev. (n)	0.0678
R(calc.)	0.190
st.dev.(D1298:12b)	0.1786
R(D1298:12b)	0.5

Lab 575: first reported 9.6 Lab 995: first reported 8.1



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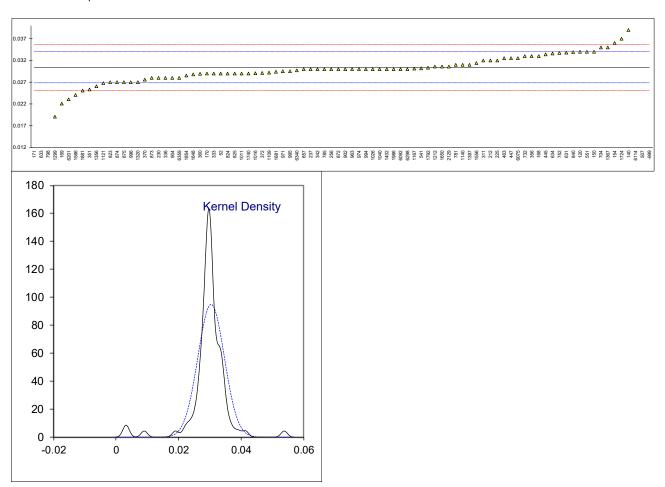
Determination of Ash Content on sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D482	0.029		-0.79	904	D482	0.028		-1.35
120	D482	0.034		2.01	913	D402			-1.00
			_						
140	D482	0.039	С	4.81	914				
150	D482	0.034		2.01	962				
154	D482	0.036		3.13	963	ISO6245	0.030		-0.23
159					971	ISO6245	0.0295		-0.51
168	D482	0.033		1.45	974	D482	0.030		-0.23
169	D482	0.022		-4.71	994	D482	0.030		-0.23
170	D482	0.02895		-0.82	995	ISO6245	0.0295		-0.51
171	ISO6245	0.003	R(0.01)	-15.35	996	D482	0.027		-1.91
175	.0002.0		(0.0.)		997	2.02			
212	ISO6245	0.032		0.89	1011	ISO6245	0.029		-0.79
225	D482	0.032		0.89	1016	D482	0.02906		-0.76
230	ISO6245	0.028		-1.35	1026	D482	0.030		-0.23
237	D482	0.03		-0.23	1040	ISO6245	0.03		-0.23
238					1065				
253					1108				
256	D482	0.03		-0.23	1109	D482	0.0292		-0.68
273					1121	ISO6245	0.0268		-2.02
309					1126				
311	D482	0.032		0.89	1134				
313	2.02				1140	IP4	0.031		0.33
323					1167	ISO6245	0.03011		-0.17
333	ISO6245	0.029		-0.79	1205	1000243			-0.17
	1506245					1000045			
334	1000045			4.05	1212	ISO6245	0.0306		0.11
336	ISO6245	0.028		-1.35	1213				
339					1277				
342	ISO6245	0.030		-0.23	1299	D482	0.019		-6.39
349					1320	ISO6245	0.027		-1.91
351	ISO6245	0.0253		-2.86	1356	ISO6245	0.026		-2.47
356	ISO6245	0.033		1.45	1367	IP4	0.035		2.57
360	ISO6245	0.0289		-0.85	1381				
370	ISO6245	0.0276		-1.57	1397	ISO6245	0.031		0.33
372	ISO6245			-0.73	1402	IP4	0.030		-0.23
	1300245	0.0291						D(0.04)	
381	10.4			4.07	1510	ISO6245	5.050	R(0.01)	2810.97
445	IP4	0.0334		1.67	1556	ISO6245	0.0314		0.55
447	IP4	0.0325		1.17	1585				
463	ISO6245	0.0325		1.17	1586	ISO6245	0.024	С	-3.59
495					1631				
507	ISO6245	0.0538		13.10	1635				
541	D482	0.0302		-0.12	1648	ISO6245	0.0288		-0.90
551	D482	0.034		2.01	1650	D482	0.0306		0.11
558					1681	ISO6245	0.0294		-0.57
575					1720	1000210			
610					1724	D482	0.037		3.69
621					1740		0.037		-0.79
	D402	0.0000		4.00		D482			
631	D482	0.0338	D(0.04)	1.90	1776	100001=			
633	D482	0.0034	R(0.01)	-15.13	1792	ISO6245	0.0303		-0.06
634	D482	0.03359		1.78	1796				
657	D482	0.030		-0.23	1854	ISO6245	0.0285		-1.07
704	ISO6245	0.035		2.57	1857				
732	D482	0.033		1.45	1881	D482	0.025		-3.03
752	D482	0.0337		1.84	1906				
753					1949				
778					1986	ISO6245	0.030		-0.23
781	ISO6245	0.031		0.33	2129	IP4	0.0306		0.11
	ISO6245			-0.23	6054	IF 4			
785		0.03	D(0.04)			1000045			
798	D482	0.009	R(0.01)	-11.99	6075	ISO6245	0.0325		1.17
823	ISO6245	0.027		-1.91	6092	ISO6245	0.03		-0.23
824	ISO6245	0.029		-0.79	6112				
825	D482	0.029		-0.79	6114	D482	0.0414		6.15
840	D482	0.0339		1.95	6201	ISO6245	0.023		-4.15
872	ISO6245	0.030		-0.23	6238				
873	D482	0.028		-1.35	6262				
874	ISO6245	0.027		-1.91	6298	D482	0.030		-0.23
875	D482	0.027		-1.91	6340	D482	0.0297		-0.40
887	D TOL	0.027		-1.51	6359	D482	0.028		-1.35
902	D482	0.030		-0.23	0008	D+02	0.020		-1.55
902	D+02	0.030		-0.23	I				

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Lab 140 first reported 0.016 Lab 1586 first reported 0.014



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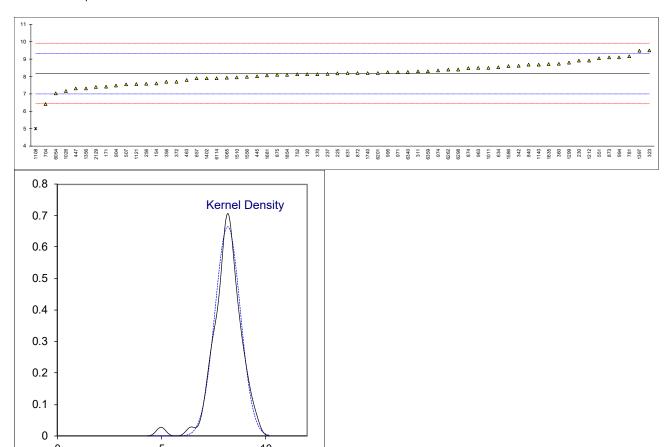
Determination of Asphaltenes on sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904	IP143	7.48		-1.19
120	D6560	8.127		-0.08	913				
140	B0000				914				
150	Docoo				962	ID440			0.50
154	D6560	7.6		-0.99	963	IP143	8.5		0.56
159					971	IP143	8.24		0.11
168					974	IP143	8.34		0.28
169					994	D6560	9.1		1.58
170					995	IP143	8.235		0.10
171	IP143	7.4		-1.33	996				
175					997				
212					1011	IP143Mod.	8.5		0.56
	Defen					ii 143iviou.	0.5		
225	D6560	8.17		-0.01	1016	ID440			
230	IP143	8.906		1.25	1026	IP143	7.15		-1.76
237	D6560	8.14		-0.06	1040				
238					1065	D6560	7.92		-0.44
253					1108	D6560	4.98	R(0.01)	-5.47
256	IP143	7.58		-1.02	1109				
273					1121	IP143	7.563		-1.05
309					1126				
311	IP143	8.3		0.21	1134				
	11 143					ID442	8.68		
313	ID440				1140	IP143	0.00		0.86
323	IP143	9.5		2.27	1167				
333					1205				
334					1212	IP143	8.91		1.26
336					1213				
339					1277				
342	IP143	8.615		0.75	1299	IP143	8.8		1.07
349					1320				
351					1356	D6560	7.3		-1.50
	ID440	 7 7		0.04		D0300	1.3		
356	IP143	7.7		-0.81	1367				
360	IP143	8.73		0.95	1381				
370	IP143	8.13		-0.08	1397	D6560	9.47		2.22
372	IP143	7.7		-0.81	1402	IP143	7.9		-0.47
381					1510	IP143	7.95		-0.39
445	IP143	8.01		-0.28	1556	IP143	7.97		-0.35
447	IP143	7.3		-1.50	1585				
463	IP143	7.79		-0.66	1586	IP143	8.6		0.73
	IF 143					IF 143			
495	ID440	 			1631	Docoo			
507	IP143	7.55		-1.07	1635	D6560	8.71		0.92
541					1648				
551	IP143	9.05		1.50	1650				
558					1681	IP143	8.06		-0.20
575					1720				
610					1724				
621					1740	D6560	8.2		0.04
	Desen	9.10				D0000			
631	D6560	8.19		0.03	1776				
633	Docoo	0.50	0	0.50	1792				
634	D6560	8.52	С	0.59	1796				
657	IP143	7.90		-0.47	1854	IP143	8.1		-0.13
704	IP143	6.41		-3.02	1857				
732					1881				
752	INH-642	8.1179		-0.10	1906				
753	• .=				1949				
778					1986				
	ID440					ID440	7 200		4.04
781	IP143	9.16		1.69	2129	IP143	7.392		-1.34
785					6054	D6560	7.0311		-1.96
798					6075				
823					6092				
824					6112				
825					6114	IP143	7.90		-0.47
840	D6560	8.67		0.85	6201	IP143	8.2		0.04
872	IP143	8.2		0.03	6238				
						ID1/12			
873	IP143	9.1		1.58	6262	IP143	8.39		0.37
874	IP143	8.48		0.52	6298	IP143	8.40		0.38
875	IP143	8.1		-0.13	6340	IP143	8.26		0.14
887					6359	IP143	8.3		0.21
902									

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normality	OK
n	61
outliers	1
mean (n)	8.175
st.dev. (n)	0.6001
R(calc.)	1.680
st.dev.(IP143:04)	0.5840
R(IP143:04)	1.635

Lab 634 first reported 10.32



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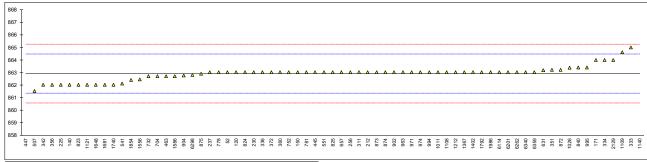
Determination of Calculated Carbon Aromaticity Index on sample #20250

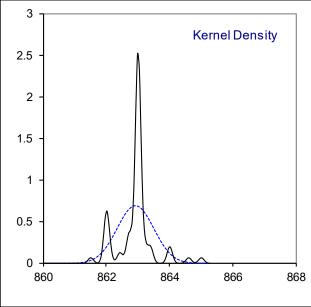
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	ISO8217	863		0.11	904	ISO8217	862.76		-0.20
120	ISO8217	863		0.11	913				
			<u></u>						
140	ISO8217	862	С	-1.16	914				
150	ISO8217	863		0.11	962				
154					963	ISO8217	863		0.11
159					971	ISO8217	863		0.11
168					974	ISO8217	863		0.11
169					994	ISO8217	863		0.11
170	100001=				995	ISO8217	863.4		0.62
171	ISO8217	864		1.38	996				
175					997				
212	ISO8217	863		0.11	1011	ISO8217	863		0.11
225	ISO8217	862		-1.16	1016				
230	ISO8217	863		0.11	1026	ISO8217	863.36		0.57
237	ISO8217	863		0.11	1040				
238	1000217				1040				
						1000047			
253					1108	ISO8217	863		0.11
256	ISO8217	863		0.11	1109	ISO8217	864.6		2.15
273					1121	ISO8217	862		-1.16
309					1126				
311	ISO8217	863		0.11	1134				
313	1000217				1140	ISO8217		D(0.01)	
						1300217	943	R(0.01)	101.93
323					1167				
333	ISO8217	865		2.66	1205				
334	ISO8217	864		1.38	1212	ISO8217	863		0.11
336	ISO8217	863		0.11	1213				
339					1277				
342	ISO8217	862		-1.16	1299				
349	1000217			-1.10	1320				
	1000017								
351	ISO8217	863.20		0.36	1356				
356	ISO8217	862		-1.16	1367	ISO8217	863		0.11
360	ISO8217	863		0.11	1381				
370					1397				
372	ISO8217	863		0.11	1402	ISO8217	863		0.11
381	1000211				1510	1000211			
445	ISO8217	863		0.11	1556	ISO8217	862.45		-0.59
			D(0.04)			1500217			-0.59
447	ISO8217	851	R(0.01)	-15.16	1585				
463	ISO8217	862.7		-0.27	1586	ISO8217	862.7		-0.27
495					1631				
507	ISO8217	861.5		-1.80	1635				
541	ISO8217	862.1		-1.04	1648	ISO8217	862		-1.16
551	ISO8217	863		0.11	1650				
558	1000211				1681	ISO8217	862.0		-1.16
575					1720	1000217			-1.10
610					1724	100001=			
621					1740	ISO8217	862		-1.16
631	ISO8217	863.19		0.35	1776				
633					1792	ISO8217	863		0.11
634					1796				
657	ISO8217	863		0.11	1854	ISO8217	862.4		-0.65
704	ISO8217	862.7		-0.27	1857				
732	ISO8217	862.7		-0.27	1881				
752	ISO8217	863		0.11	1906				
753					1949				
778	ISO8217	863		0.11	1986	ISO8217	863		0.11
781	ISO8217	863		0.11	2129	ISO8217	864		1.38
785					6054				
798					6075				
823	ISO2217	862			6092				
	ISO8217			-1.16					
824	ISO8217	863		0.11	6112				
825	ISO8217	863		0.11	6114	ISO8217	863		0.11
840	ISO8217	863.4		0.62	6201	ISO8217	863		0.11
872	ISO8217	863.2		0.36	6238				
873	ISO8217	863		0.11	6262	ISO8217	863		0.11
874	ISO8217	863		0.11	6298	ISO8217	862.8		-0.14
875	ISO8217	862.9		-0.02	6340	ISO8217	863		0.11
887	1000047				6359	ISO8217	863		0.11
902	ISO8217	863		0.11	1				

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normality	not OK
n	69
outliers	2
mean (n)	862.914
st.dev. (n)	0.5791
R(calc.)	1.621
st.dev.(ISO8217:17)	0.7857
R(ISO8217:17)	2.2

Lab 140 first reported 856





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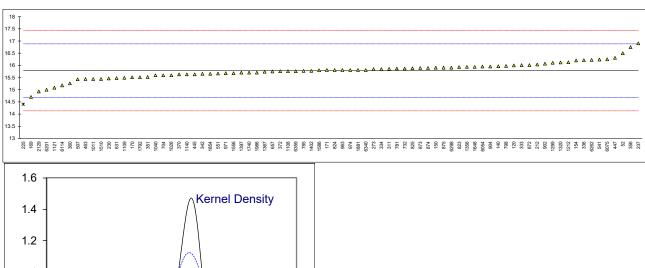
Determination of Carbon Residue micro method on sample #20250; results in %M/M

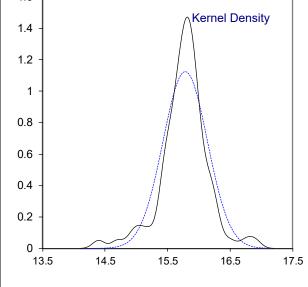
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4530	16.5	mark	1.30	904	ISO10370	15.95	mun	0.30
	D4530					13010370			
120		16.00		0.39	913				
140	ISO10370	15.96		0.32	914				
150	D4530	15.9		0.21	962				
154	D4530	16.2		0.76	963	ISO10370	15.80		0.03
159					971	ISO10370	15.67		-0.21
168					974	D4530	15.8		0.03
169	D4530	14.7		-1.97	994				
170	D4530	15.5		-0.52	995				
171	ISO10370	15.80		0.03	996				
175					997				
212	ISO10370	16.03		0.45	1011	ISO10370	15.43		-0.64
225	D4530	14.4	R(0.05)	-2.51	1016	10010010			
230	ISO10370	15.46	11(0.00)	-0.59	1026	D4530	15.59	С	-0.35
237	D4530	16.90		2.03	1040	ISO10370	15.585	O	-0.36
238	D4330	10.90		2.03	1040	130 10370			-0.30
						10040070	45.70		
253					1108	ISO10370	15.76		-0.04
256					1109	D4530	15.486		-0.54
273	D4530	15.84		0.10	1121	ISO10370	15.072		-1.29
309					1126				
311	D4530	15.85		0.12	1134				
313					1140	IP398	15.62		-0.30
323					1167				
333	ISO10370	16.01		0.41	1205				
334	ISO10370	15.84		0.10	1212	ISO10370	16.130		0.63
336	ISO10370	16.21		0.77	1213				
339	10010010				1277				
342	ISO10370	15.65		-0.24	1299		16.10		0.57
349	130 10370			-0.24	1320	ISO10370	16.10		0.59
	ISO10370	15.522							
351				-0.48	1356	ISO10370	15.93		0.26
356	ISO10370	16.75		1.75	1367	IP398	15.73		-0.10
360	ISO10370	15.25		-0.97	1381	100100-0			
370	ISO10370	15.62		-0.30	1397	ISO10370	15.7		-0.15
372	ISO10370	15.76		-0.04	1402	IP398	15.77		-0.03
381					1510	ISO10370	15.44		-0.62
445	IP398	15.63		-0.28	1556	ISO10370	15.67		-0.21
447	IP398	16.304		0.94	1585				
463	ISO10370	15.429		-0.64	1586	D4530	15.79		0.01
495					1631				
507	ISO10370	15.425		-0.65	1635				
541	D4530	16.23		0.81	1648	ISO10370	15.93		0.26
551	D4530	15.66		-0.23	1650				
558	D-1000	10.00			1681				
575					1720				
610					1724			W	
						D4E30	15.70	VV	0.15
621	D4520	45.47		0.57	1740	D4530			-0.15
631	D4530	15.47		- 0.57	1776	10040070	45.50		0.50
633					1792	ISO10370	15.50		-0.52
634	100400=0	45.75			1796	100405=0	45.05		
657	ISO10370	15.75		-0.06	1854	ISO10370	15.65		-0.24
704	ISO10370	15.59		-0.35	1857				
732	D4530	15.86		0.14	1881	ISO10370	15.8		0.03
752					1906				
753					1949				
778					1986	ISO10370	15.7		-0.15
781	ISO10370	15.86		0.14	2129	IP398	14.926		-1.56
785	ISO10370	15.77		-0.03	6054	D4530	15.9496		0.30
798	D4530	15.9765		0.35	6075	ISO10370	16.245		0.84
823	ISO10370	15.92		0.25	6092				
824	ISO10370	15.8		0.03	6112				
825	ISO10370	15.88		0.03	6114	D4530	15.17		-1.11
840	10010010	13.00			6201	D4530	14.995		-1.11
	ISO10270					D4000			
872	ISO10370	16.01		0.41	6238	D4520	16.22		0.70
873	ISO10370	15.89		0.19	6262	D4530	16.22		0.79
874	D4530	15.89		0.19	6298	D4530	15.90		0.21
875	D4530	15.90		0.21	6340	D4530	15.80		0.03
887	100400=0	40.07			6359	D4530	15.76		-0.04
902	ISO10370	16.07		0.52	İ				

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normality	not OK
n	79
outliers	1
mean (n)	15.7841
st.dev. (n)	0.35510
R(calc.)	0.9943
st.dev.(ISO10370:14)	0.55081
R(ISO10370:14)	1.5423
compare	
R(D4530:15)	0.8793

Lab 1026 first reported 17.86 Lab 1724 test result withdrawn, reported 17.63





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Determination of Conradson Carbon Residue on sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904				
120					913				
140					914				
150					962	D400	40.40		0.00
154					963	D189	16.48		0.60
159 168					971 974	D189 D189	15.87 15.9		-0.08 -0.05
169					994	D189	16.1		0.17
170					995	D189	16.251		0.17
171	D189	14.1	R(0.05)	-2.06	996	D189	16.48		0.60
175	2.00		(0.00)		997	2.00			
212					1011				
225					1016				
230	D189	15.24	С	-0.79	1026				
237	D189	15.3		-0.72	1040				
238					1065				
253	D400	 1E C		0.20	1108				
256 273	D189	15.6		-0.38	1109 1121				
309					1121				
311					1134				
313					1140				
323					1167				
333					1205				
334					1212				
336					1213				
339					1277				
342					1299				
349					1320				
351 356					1356 1367				
360	D189	15.45		-0.55	1381				
370	D103			-0.55	1397				
372	D189	15.86		-0.09	1402	IP13	17.4		1.63
381					1510				
445	IP13	16.58		0.71	1556				
447					1585				
463					1586	D189	16.07		0.14
495	D.100	45.04			1631				
507	D189	15.94		0.00	1635				
541 551	D189 D189	15.99 15.66		0.05 -0.32	1648 1650	D189	16.0	С	0.06
558	D109	15.00		-0.32	1681	D189	15.77	C	-0.19
575	D189	18.65	C,R(0.01)	3.02	1720	D 103			-0.10
610	2.00		0,. 1(0.01)		1724				
621					1740	D189	15.85		-0.10
631					1776				
633					1792				
634	D189	15.289		-0.73	1796				
657	D400	45.70		0.47	1854	D4530	15.95		0.01
704 732	D189	15.79		-0.17 	1857 1881	D189	16.0		0.06
752 752					1906	D109	10.0		0.00
753					1949				
778					1986	D189	16.0		0.06
781	D189	15.92		-0.03	2129	D189	14.0	R(0.05)	-2.17
785					6054			,	
798					6075				
823	D189	16.46		0.58	6092				
824					6112				
825	D400	44.70		4.00	6114				
840	D189	14.76		-1.32	6201				
872 873					6238 6262				
873 874					6298	D189	16.40		0.51
875					6340	D 100			
887					6359				
902									
				l.					

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 normality
 not OK

 n
 29

 outliers
 3

 mean (n)
 15.9434

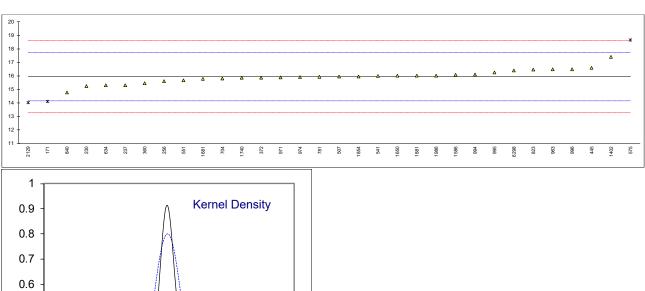
 st.dev. (n)
 0.49933

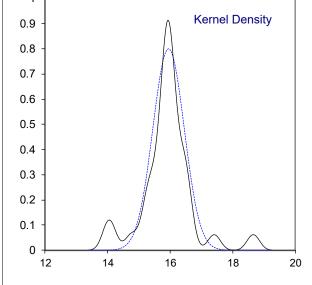
 R(calc.)
 1.3981

 st.dev.(D189:06)
 0.89546

 R(D189:06)
 2.5073

Lab 230 first reported 21.817 Lab 575 first reported 20.08 Lab 1650 first reported 21.25





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Determination of Density at 15°C on sample #20250; results in kg/m³

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4052	1008		-0.17	904	ISO12185	1008.0		-0.17
120	D4052	1008.0		-0.17	913	10012100			
140	D4052	1000.0		-2.04	914				
150	D1298	1009.4		2.44	962	10040405	4007.0		
154	D4052	1009		1.69	963	ISO12185	1007.9		-0.36
159					971	ISO12185	1008.1		0.01
168					974	D1298	1008.2		0.20
169	D1298	1007.9		-0.36	994	ISO12185	1008.0		-0.17
170	D4052	1008.12		0.05	995	ISO12185	1008.1		0.01
171	ISO12185	1008.6		0.95	996	D1298	1009		1.69
175					997	ISO12185	1008.2		0.20
212	ISO12185	1008.7		1.13	1011	ISO12185	1008.4		0.57
225	D4052	1007.5		-1.11	1016				
230	ISO12185	1008.0		-0.17	1026	D4052	1008.4		0.57
237	D4052	1007.6		-0.92	1040	ISO12185	1008.5		0.76
238	D1298	1007.0		0.20	1040	D4052	1008.8		1.32
253	D4052	1006.7		-2.60	1108	ISO12185	1008.8		1.32
256	D1298	1008.5		0.76	1109	D4052	1007.8		-0.55
273	D1298	1007.5		-1.11	1121	ISO12185	1007.7		-0.73
309					1126				
311	D4052	1007.8		-0.55	1134				
313	ISO12185	1007.8		-0.55	1140	IP365	1008.2		0.20
323	ISO12185	1008.4		0.57	1167	ISO12185	1008.0		-0.17
333	ISO12185	1008.3		0.39	1205				
334	ISO12185	1008.3		0.39	1212	ISO12185	1007.8		-0.55
336	ISO12185	1008.4		0.57	1213	D4052	1008.1		0.01
339	10012100				1277	D1298	1016.1	R(0.01)	14.95
342	D4052	1007.8		-0.55	1299	D4052	1000.8	R(0.01)	-13.61
349	D4032			-0.55	1320	ISO12185	1000.0	11(0.01)	2.07
	ISO3675								
351		1008.30		0.39	1356	ISO12185	1007.9		-0.36
356	ISO12185	1007.8		-0.55	1367	IP365	1007.5		-1.11
360	ISO12185	1008.4		0.57	1381	ISO12185	1008.26		0.31
370	ISO12185	1008.4		0.57	1397	ISO12185	1008.9		1.51
372	ISO12185	1008.0		-0.17	1402	IP365	1008.6		0.95
381	ISO12185	1007.2	С	-1.67	1510	ISO12185	1008.0		-0.17
445	IP365	1008.7		1.13	1556	ISO12185	1007.3		-1.48
447	IP365	996.2	R(0.01)	-22.20	1585				
463	ISO12185	1007.81	, ,	-0.53	1586	ISO12185	1007.8		-0.55
495	ISO12185	1008.50		0.76	1631	ISO12185	1004.25	R(0.01)	-7.17
507	ISO12185	1007.9		-0.36	1635			,	
541	ISO12185	1007.25		-1.57	1648	ISO12185	1007.45		-1.20
551	D4052	1008.2		0.20	1650	D4052	1007.8		-0.55
558	2.002				1681	ISO12185	1007.71		-0.72
575					1720	10012100	1007.71		-0.72
610					1724			W	
621					1740	D4052	1007.5	VV	-1.11
631	D4052								
		1008.36	D(0.04)	0.50	1776	ISO12185	1007.64		-0.85
633	D1298	1014.9	R(0.01)	12.71	1792	ISO12185	1008.3		0.39
634	D1298	1008.1		0.01	1796	10040405	4007.7		
657	ISO12185	1007.9		-0.36	1854	ISO12185	1007.7		-0.73
704	ISO12185	1007.9		-0.36	1857				
732	ISO12185	1007.90		-0.36	1881	ISO12185	1008.5		0.76
752	ISO3675	1008.1		0.01	1906				
753	ISO12185	1008.0		-0.17	1949				
778	ISO12185	1008.1		0.01	1986	D1298	1008.4		0.57
781	ISO12185	1008.1		0.01	2129	D4052	1008.0		-0.17
785	ISO12185	1008.5		0.76	6054				
798	D1298	1008.1	С	0.01	6075				
823	ISO12185	1007.7	•	-0.73	6092	ISO12185	1008.0		-0.17
824	ISO12185	1007.7		-0.36	6112	ISO12185	1007.50		-1.11
825	ISO12185	1007.9		-0.36	6114	ISO12185	1007.30		0.01
840								C	
	ISO12185	1008.82		1.36	6201	D4052	1008.0	С	-0.17
872	ISO12185	1008.3		0.39	6238	D4052	1000.0		0.47
873	ISO12185	1008.5		0.76	6262	D4052	1008.0		-0.17
874	ISO12185	1008.2		0.20	6298	D4052	1008.0		-0.17
875	ISO12185	1008.3		0.39	6340	IP365	1008.2	_	0.20
887					6359	D4052	1008.4	С	0.57
902	D1298	1008.1		0.01	I				

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 normality
 suspect

 n
 101

 outliers
 5

 mean (n)
 1008.093

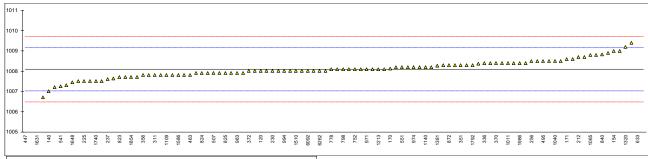
 st.dev. (n)
 0.4463

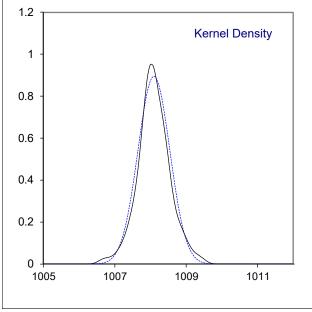
 R(calc.)
 1.250

 st.dev.(ISO12185:96)
 0.5357

 R(ISO12185:96)
 1.5

Lab 381 first reported 958.3 Lab 798 first reported 1.0081 kg/m3 Lab 1724 test result withdrawn, reported 1.0044 kg/L Lab 6201 first reported 1.008 kg/m3 Lab 6359 first reported 1.0084 kg/m3





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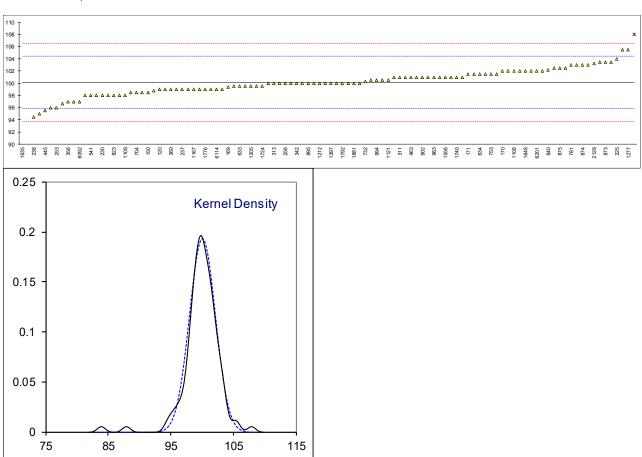
Determination of Flash Point PMcc on sample #20250; results in °C

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D93-B	98.0		-1.01	904	ISO2719-B	101		0.39
120	D93-A	99.0		-0.54	913	.00202			
140	D93-B	101.5		0.63	914				
150	D93-B	98.5		-0.77	962				
154	D93-B	99.0		-0.54	963	ISO2719-B	101.0		0.39
159	D00 D				971	ISO2719-B	101.0		0.39
168	D93-B	101.5		0.63	974	D93-B	100.0		-0.07
169	D93-B	99.4		-0.35	994	D93-B	100.5		0.16
170	D93-B	102.0		0.86	995	ISO2719-B	100.0		-0.07
171	ISO2719-A	101.5		0.63	996	D93-B	99.0		-0.54
175	D93-B	99		-0.54	997	ISO2719-B	100.0		-0.07
212	ISO2719-B	96.7		-1.61	1011	ISO2719-B	100.5		0.16
225	D93-B	104.0		1.79	1011	13027 19-15			0.10
230	ISO2719-B	98.0		-1.01	1026	ISO2719-B	103.5		1.56
237	D93-B	99.0		-0.54	1040	ISO2719-B	98.0		-1.01
238	D93-B	99.0 94.5		-0.54 -2.64	1040	13027 19-A	90.0		-1.01
		94.5 96				1800710 B			
253	D93-B			-1.94	1108	ISO2719-B	102.0		0.86
256	D93-B	100.0		-0.07	1109	D93-A	98.0		-1.01
273					1121	ISO2719-B	100.53		0.17
309	D00 D	404.0			1126				
311	D93-B	101.0		0.39	1134	IDO4 D			
313	D93-B	100.0		-0.07	1140	IP34-B	99.5		-0.31
323	ISO2719-A	98.5		-0.77	1167	ISO2719-B	99.0		-0.54
333	ISO2719-B	100.5		0.16	1205	D93-B	99.5		-0.31
334	ISO2719-B	99.5		-0.31	1212	ISO2719-B	100.0		-0.07
336	ISO2719-B	100.0		-0.07	1213	D93-B	103		1.33
339					1277	D93-A	105.5		2.49
342	ISO2719-B	100.0		-0.07	1299	D93-B	100.0		-0.07
349					1320				
351	ISO2719-B	101.00		0.39	1356	ISO2719-B	102.5		1.09
356	ISO2719-B	97.0		-1.47	1367	D93-B	99.5		-0.31
360	ISO2719-B	99.0		-0.54	1381				
370	D93-B	100.0		-0.07	1397	D93-B	100.0		-0.07
372	ISO2719-B	101.0		0.39	1402	IP34-B	102.0		0.86
381					1510	ISO2719-B	101.5		0.63
445	D93-B	95.5		-2.17	1556	ISO2719-B	101.0		0.39
447	D93-B	95.0		-2.41	1585				
463	ISO2719-B	101.0		0.39	1586	D93-B	99.0		-0.54
495	ISO2719-B	98.5		-0.77	1631	D93-B	98.8		-0.63
507	ISO2719-B	88.00	R(0.01)	-5.67	1635	ISO2719-A	84	R(0.01)	-7.54
541	D93-B	98.00		-1.01	1648	ISO2719-B	102.0		0.86
551	D93-B	103.0	С	1.33	1650	D93-B	101.0		0.39
558					1681	ISO2719-B	100.0		-0.07
575	D93-B	101	С	0.39	1720				
610					1724	D93-B	99.5		-0.31
621					1740	D93-B	101.0		0.39
631	D93-B	96.0		-1.94	1776	ISO2719-B	99.0		-0.54
633	D93-B	99.50		-0.31	1792	ISO2719-C	100.0		-0.07
634	D93-B	101.5		0.63	1796				
657	D93-B	100		-0.07	1854	ISO2719-B	100		-0.07
704	D93-B	98.5		-0.77	1857				
732	D93-B	100.3		0.07	1881	ISO2719-B	100.0		-0.07
752	D93-B	105.5		2.49	1906				
753	ISO2719-B	101.5		0.63	1949				
778	ISO2719-B	103.5		1.56	1986	ISO2719-B	99.0		-0.54
781	ISO2719-B	103.0		1.33	2129	IP34-B	103.26		1.45
785	ISO2719-B	102.0		0.86	6054	D93-B	97.0		-1.47
798	D93-B	108.0	R(0.05)	3.66	6075	ISO2719-B	102.0		0.86
823	ISO2719-B	98.0	11(0.00)	-1.01	6092	D93-B	97	С	-1.47
824	ISO2719-B	98.0		-1.01	6112	- 30 B		Ŭ	-1
825	ISO2719-B	98.0		-1.01	6114	D93-B	99.0		-0.54
840	D93-B	102.2		0.95	6201	D93-B	102		0.86
872	ISO2719-B	102.5		1.09	6238	500 5			
873	D93-B	103.5		1.56	6262	D93-B	99.0		-0.54
874	D93-B	103.0		1.33	6298	D93-B	102.0		0.86
875	D93-B	102.5		1.09	6340	D93-B	102.0		0.39
887	500-D	102.5		1.09	6359	D93-B	101.0		-0.07
902	ISO2719-B	101.0		0.39		D00-D	100		-0.01
302	1002110-0	101.0		0.09	l				

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normality	OK
n	105
outliers	3
mean (n)	100.159
st.dev. (n)	2.0618
R(calc.)	5.773
st.dev.(ISO2719-B:16)	2.1429
R(ISO2719-B:16)	6

Lab 551 first reported 90 Lab 575 first reported 108 Lab 6092 first reported 92



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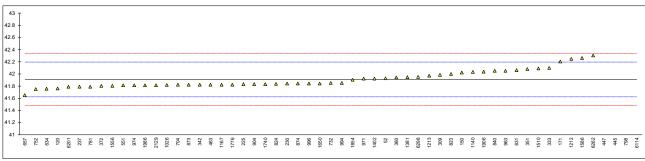
Determination of Heat of Combustion (Gross) on sample #20250; results in MJ/kg

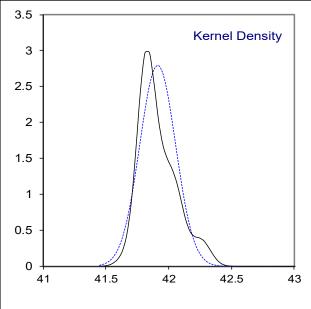
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D240	41.925	С	0.11	904	D4868	41.83	··········	-0.56
120	D4868	41.76	Č	-1.05	913	D-1000			0.00
140	D-1000		J		914				
150	D240	42.022		0.78	962				
154	D240				963	D240	42.05		0.98
154					971	D240 D240	41.92		0.96
168					974	D4868	41.81		-0.70
169					994	D4868	41.85		-0.42
170	D040	40.005			995	D 4000	44.04		0.40
171	D240	42.205		2.07	996	D4868	41.84		-0.49
175					997				
212	D 4000				1011				
225	D4868	41.83		-0.56	1016	D 4000	44.040		
230	D4868	41.84		-0.49	1026	D4868	41.816		-0.66
237	D4868	41.790		-0.84	1040				
238					1065				
253					1108				
256					1109				
273					1121				
309	D240	41.985		0.53	1126				
311					1134				
313					1140	ISO8217	42.03		0.84
323					1167	DIN51900-2	41.820		-0.63
333	D240	42.100		1.33	1205				
334					1212		42.245		2.35
336					1213		41.97		0.42
339					1277				
342	D4868	41.82		-0.63	1299				
349					1320				
351	D4868	42.080		1.19	1356				
356					1367				
360	D240	41.938		0.20	1381		41.946		0.25
370					1397				
372	D4868	41.80		-0.77	1402	IP2	41.92		0.07
381					1510		42.09		1.26
445	D240	46.064	R(0.01)	29.08	1556	D4868	41.80		-0.77
447	D240	43.9374	R(0.01)	14.19	1585	2 .000			
463	D4868	41.82	11(0.01)	-0.63	1586	D240	42.258		2.44
495	2.000				1631	22.0			
507					1635				
541					1648				
551	D4868	41.81	С	-0.70	1650	D4868	41.84		-0.49
558	D-1000		O	-0.70	1681	D-1000			-0.43
575					1720				
610					1724				
621					1740	D240	41.830		-0.56
631		42.0599		1.05	1776	D4868	41.82		-0.63
633					1770	D4000			
634	D240	 41.755		-1.08	1792				
						D240	41.90		0.07
657	DIN51900-1	41.650		-1.82	1854	D240			-0.07
704	D4868	41.82		-0.63	1857				
732	D4868	41.849		-0.43	1881	D 4000	40.000	0	0.00
752	D4868	41.75		-1.12	1906	D4809	42.038	С	0.90
753					1949	D 4000			
778					1986	D4868	41.810		-0.70
781	D4868	41.79		-0.84	2129	D240	41.810		-0.70
785					6054				
798		50.42	R(0.01)	59.57	6075				
823	KS M2057	41.999		0.62	6092				
824	KS M2057	41.836		-0.52	6112				
825					6114	D4868	50.45	R(0.01)	59.78
840	D240	42.050		0.98	6201	D240	41.786		-0.87
872					6238				
873	D4868	41.82		-0.63	6262	D240	42.3046		2.76
874	D4868	41.84		-0.49	6298	D240	41.950		0.28
875					6340				
887					6359				
902									

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normality	suspect
n	53
outliers	4
mean (n)	41.9100
st.dev. (n)	0.14257
R(calc.)	0.3992
st.dev.(D240:19)	0.14286
R(D240:19)	0.40

Lab 52 first reported 41.355 Lab 120 first reported 40.72 Lab 551 first reported 50.31 Lab 1906 first reported 42.148





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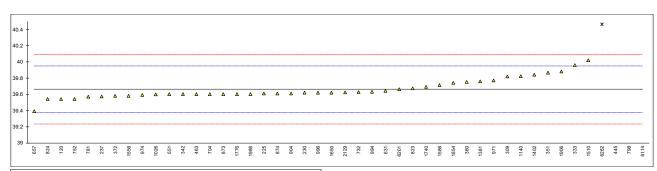
Determination of Heat of Combustion (Net) on sample #20250; results in MJ/kg

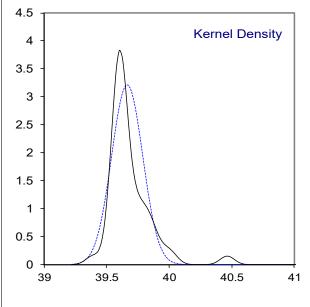
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904	D4868	39.61		-0.38
120	D4868	39.54	С	-0.87	913				
140					914				
150					962				
154					963				
159					971	D240	39.77		0.74
168					974	D4868	39.59		-0.52
169					994	D4868	39.63		-0.24
170					995	D. 4000			
171					996	D4868	39.62		-0.31
175					997				
212					1011				
225	D4868	39.61		-0.38	1016				
230	D4868	39.62		-0.31	1026	D4868	39.599		-0.45
237	D4868	39.573		-0.64	1040				
238					1065				
253					1108				
256					1109				
273					1121				
309	D240	39.820		1.09	1126				
311	D2-10				1134				
313					1140	ISO8217	20 0217154		
						1300217	39.8217154		1.11
323	D040			0.07	1167				
333	D240	39.960		2.07	1205				
334					1212				
336					1213				
339					1277				
342	D4868	39.60		-0.45	1299				
349					1320				
351	D4868	39.866		1.42	1356				
356					1367				
360	D240	39.753		0.62	1381		39.759		0.67
370					1397				
372	D4868	39.58		-0.59	1402	IP2	39.84		1.23
381	B 1000				1510		40.02		2.49
445	D240	43.963	R(0.01)	30.09	1556	D4868	39.58		-0.59
447	D240		11(0.01)		1585	D4000			-0.55
463	D4868	39.60		-0.45	1586	D240	39.712		0.34
	D4000					D240			0.34
495					1631				
507					1635				
541	D 4000		_		1648	D. 4000			
551	D4868	39.60	С	-0.45	1650	D4868	39.62		-0.31
558					1681				
575					1720				
610					1724				
621					1740	D240	39.690		0.18
631		39.6424		-0.15	1776	D4868	39.60		-0.45
633					1792				
634					1796				
657	DIN51900-1	39.390		-1.92	1854	D240	39.74		0.53
704	D4868	39.60		-0.45	1857				
732	D4868	39.625		-0.27	1881				
752	D4868	39.54		-0.87	1906	D4809	39.880	С	1.51
753	D-1000			-0.07	1949	D-1003		O	
778					1986	D4868	39.600		-0.45
781	D4868	39.57		-0.66	2129	D240			
	D4000					D240	39.624		-0.28
785		45.40	D(0.04)		6054				
798	1/0 1/0057	45.12	R(0.01)	38.19	6075				
823	KS M2057	39.672		0.06	6092				
824	KS M2057	39.539		-0.87	6112				
825					6114	D4868	45.15	R(0.01)	38.40
840					6201	D240	39.664		0.00
872					6238				
873	D4868	39.60		-0.45	6262	D240	40.4632	R(0.01)	5.60
874	D4868	39.61		-0.38	6298			•	
875					6340				
887					6359				
902									
					•				

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normality	suspect
n	42
outliers	4
mean (n)	39.6638
st.dev. (n)	0.12390
R(calc.)	0.3469
st.dev.(D189:06)	0.14286
R(D189:06)	0.40

Lab 120 first reported 38.68 Lab 551 first reported 45.32 Lab 1906 first reported 39.816





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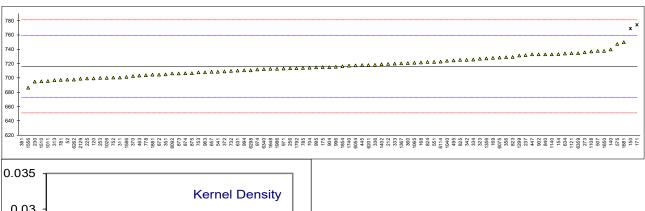
Determination of Kinematic Viscosity at 50°C on sample #20250; results in mm²/s

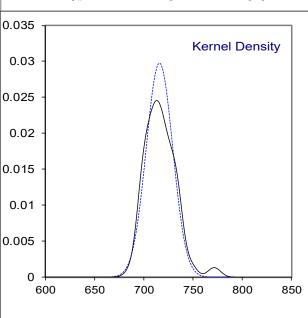
lab	method	value	mark	z(targ)	lab	method	value	mark z(targ)
52	D445	697.4		-0.86	904	ISO3104	715.0	-0.05
120	D445	699.24		-0.78	913	1000104		
			0					
140	D445	739.49	С	1.08	914			
150	D445	769.0	R(0.05)	2.44	962			
154	D445	733.0		0.78	963	ISO3104	707.8	-0.38
159					971	ISO3104	712.9	-0.15
	D44E				974	D445	711.8	
168	D445	721.3		0.24				-0.20
169	D445	727.9		0.55	994	D445	710.5	-0.26
170					995	ISO3104	714.7	-0.06
171	ISO3104	774.3	R(0.05)	2.69	996	D445	715.2	-0.04
175	D445	714.9	(/	-0.06	997			
212	ISO3104	719.5		0.16	1011	ISO3104	695.4	-0.96
						1303104		
225	D445	699.0		-0.79	1016			
230	ISO3104	694.8304		-0.98	1026	ISO3104	700.0	-0.74
237	D445	731.5		0.71	1040	ISO3104	723.65	0.35
238	2				1065	D445	721.2	0.24
	D445							
253	D445	700.00		-0.74	1108	ISO3104	736.9	0.96
256	D445	713.2		-0.13	1109			
273	D445	735.6		0.90	1121	ISO3104	734.29	0.84
309					1126			
311	D445	700.4		-0.73	1134			
						1554		
313	D445	696.7		-0.90	1140	IP71	732.9	0.78
323	ISO3104	726.6		0.49	1167			
333	ISO3104	719.6		0.16	1205			
334	ISO3104	725.3		0.42	1212			
336	ISO3104	718.1		0.09	1213			
339					1277			
342	ISO3104	725.03		0.41	1299	D445	731.0	0.69
349					1320			
	1002404					1000404		
351	ISO3104	704.70		-0.53	1356	ISO3104	727.2	0.51
356	ISO3104	728.9		0.59	1367	IP71	720.1	0.18
360	ISO3104	720.60		0.21	1381			
370	ISO3104	702.32		-0.64	1397			
372	ISO3104	708.9		-0.33	1402	ISO3104	718.9	0.13
			D(0.04)					
381	ISO3104	334.5	R(0.01)	-17.63	1510	ISO3104	694.9	-0.98
445	IP71	717.8		0.08	1556	ISO3104	685.95	-1.39
447	D445	732.8		0.77	1585			
463	ISO3104	703.16		-0.60	1586	ISO3104	701.27	-0.69
495	ISO3104	724.305		0.38	1631	1000104		
507	ISO3104	737.5		0.99	1635			
541	D445	708.405		-0.36	1648	ISO3104	712.40	-0.17
551	D445	722.3		0.29	1650	D445	737.62	0.99
558					1681	ISO3104	749.84	1.56
575	D445	747.54		1.45	1720	1000104		
	D445							
610					1724			
621					1740	D445	716.8	0.03
631	D445	709.949		-0.28	1776			
633					1792	ISO3104	713.31	-0.13
634	D445	733.9		0.82		.500104	710.01	-0.19
					1796	1000404		
657	ISO3104	708.4		-0.36	1854	ISO3104	716.1	0.00
704	D445	714.0		-0.10	1857			
732	D445	709.75		-0.29	1881	D445	704.2	-0.55
752	ISO3104	700.4		-0.73	1906			
753	ISO3104	707.8		-0.38	1949			
778	ISO3104	703.4		-0.59	1986	ISO3104	712.6	-0.16
781	ISO3104	697.2		-0.87	2129	D445	698.9	-0.80
785	ISO3104	713.6		-0.12	6054	D445	717.3	0.06
798	1000101				6075			0.57
	1000101					ISO3104	728.45	
823	ISO3104	729.0		0.60	6092	D445	705.9	-0.47
824	ISO3104	722.1		0.28	6112			
825	ISO3104	724.9		0.41	6114	D445	722.71	0.31
840	D445	732.86		0.77	6201	D445	717.8	0.08
						D440		
872	ISO3104	704.3		-0.55	6238			
873	D445	706.1		-0.46	6262	D445	697.69	-0.85
874	D445	706.5		-0.44	6298	D445	710.65	-0.25
875	ISO3104	706.5		-0.44	6340	D445	712.0	-0.19
887				-0.44	6359		734.4	0.85
	1002404				0339	D445	134.4	0.05
902	ISO3104	732.8		0.77	l			

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normality	OK
n	92
outliers	3
mean (n)	716.1035
st.dev. (n)	13.40940
R(calc.)	37.5463
st.dev.(ISO3104:20)	21.63911
R(ISO3104:20)	60.5895

Lab 140 first reported 38.68





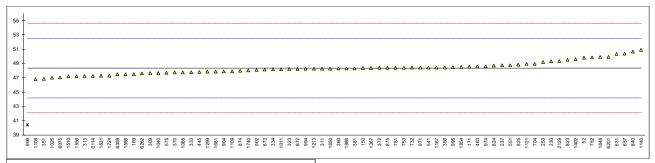
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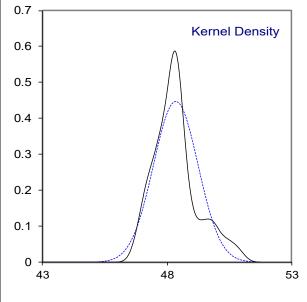
Determination of Kinematic Viscosity at 100°C on sample #20250; results in mm²/s

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D445	49.80	IIIaik	0.70	904	ISO3104	47.87	IIIaik	-0.23
120	D443				913	1003104			-0.23
140					914				
150	D445	48.33		-0.01	962				
	D445	40.33							
154 159					963 971	ISO3104	48.40		0.03
168					971	D445	48.60		0.03
169	D445	 47.48		-0.41	994	D445	48.24		-0.05
170	D445	47.40		-0.41	994	ISO3104	48.47		0.06
170	ISO3104	48.52		0.09	996	D445	40.37	R(0.01)	-3.83
171	1303104	40.32		0.09	997	D443	40.57	13(0.01)	-3.03
212					1011	ISO3104	48.18		-0.08
225					1011	1000104			-0.00
230	ISO3104	49.316		0.47	1026	ISO3104	47.01		-0.64
237	D445	48.72		0.18	1040	ISO3104	47.630		-0.34
238	D440				1065	D445	47.737		-0.29
253	D445	49.2		0.41	1108	ISO3104	46.8		-0.74
256	5440				1109	D445	47.87		-0.23
273					1121	ISO3104	48.92		0.28
309	D445	47.63		-0.34	1126	1000104			
311	D445	48.25		-0.04	1134				
313	D445	47.22		-0.54	1140	IP71	50.9		1.23
323	ISO3104	48.21		-0.06	1167	ISO3104	48.425		0.04
333	ISO3104	47.75		-0.28	1205				
334	ISO3104	48.15		-0.09	1212				
336					1213	D445	48.24		-0.05
339					1277				
342					1299	D445	47.85		-0.24
349					1320				
351	ISO3104	46.83		-0.73	1356				
356	ISO3104	48.43		0.04	1367	IP71	48.34		0.00
360	ISO3104	48.278		-0.03	1381				
370	ISO3104	47.732		-0.29	1397				
372	ISO3104	48.36		0.01	1402	ISO3104	49.57		0.59
381	ISO3104	48.31		-0.02	1510	ISO3104	47.2		-0.55
445	IP71	47.80		-0.26	1556	ISO3104	47.201		-0.55
447					1585				
463	ISO3104	48.591		0.12	1586	ISO3104	47.47		-0.42
495					1631	ISO3104	47.266		-0.52
507					1635				
541	D445	48.409		0.03	1648	ISO3104	49.892		0.74
551	D445	48.74		0.19	1650	D445	48.252		-0.04
558					1681	ISO3104	47.855		-0.23
575	D445	47.7		-0.31	1720				
610					1724	D445	47.275		-0.51
621					1740	D445	48.00		-0.16
631	D445	50.324		0.95	1776				
633					1792				
634					1796				
657	ISO3104	50.36		0.97	1854	ISO3104	48.5		0.08
704	D445	48.94		0.29	1857				
732	D445	48.392		0.02	1881				
752	D445	49.850		0.72	1906				
753 770	ISO3104	48.38		0.02	1949	1000404	40.00		0.00
778	1002404	40.00		0.00	1986	ISO3104	48.30		-0.02
781 705	ISO3104	48.38		0.02	2129	D445	49.36		0.49
785 709					6054	1002404	 47.051		0.60
798	D445	40.50		0.57	6075	ISO3104	47.051		-0.62
823 824	D445 ISO3104	49.52 48.70		0.57 0.17	6092 6112				
824 825				0.17		D445	 47.222		-0.54
825 840	ISO3104 D445	48.81 50.652		1.11	6114 6201		47.222 49.93		-0.54 0.76
840 872	ISO3104	50.652 48.22		-0.06		D445	49.93		0.76
872 873	D445	48.22 48.13		-0.06	6238 6262	D445	47.621		-0.35
673 874	D445	46.13 47.96		-0.10 -0.18	6298	D 44 0	47.021		-0.33
874 875	ISO3104	47.96 48.36		-0.18 0.01	6340				
887	1503104	40.30		0.01	6359	D445	 47.46		
902	ISO3104	48.08		-0.13	0339	D440	47.40		-0.42
902	1505104	- 0.00		-0.13	l				

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normality	OK
n	75
outliers	1
mean (n)	48.3430
st.dev. (n)	0.89263
R(calc.)	2.4994
st.dev.(ISO3104:20)	2.08220
R(ISO3104:20)	5.8302





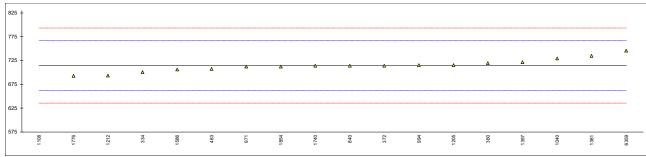
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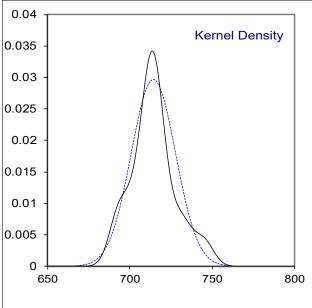
Determination of Viscosity Stabinger at 50°C on sample #20250; results in mm²/s

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904				
120 140					913 914				
150					962				
154					963				
159					971	D7042	711.8		-0.09
168					974				
169					994	D7042	715.0		0.03
170					995				
171					996				
175					997				
212 225					1011				
230					1016 1026				
237					1040	D7042	728.92		0.56
238					1065				
253					1108	D7042	509.7	G(0.01)	-7.79
256					1109				
273					1121				
309					1126				
311 313					1134 1140				
323					1140				
333					1205	D7042	715.23		0.04
334	D7042	700.2		-0.54	1212	D7042	693.25		-0.80
336					1213				
339					1277				
342					1299				
349					1320				
351					1356				
356 360	D7042	719.18		0.19	1367 1381	D7042	734.28		0.76
370	D7042	7 19.10		0.19	1397	D7042	734.20 721.1		0.76
372	D7042	713.9		-0.01	1402	D1012			
381					1510				
445					1556				
447					1585				
463	D7042	706.95		-0.28	1586	D7042	705.7		-0.33
495 507					1631 1635				
541					1648				
551					1650				
558					1681				
575					1720				
610					1724				
621					1740	D7042	713.7		-0.02
631					1776	D7042	692.75		-0.82
633 634					1792 1796				
657					1854	D7042	711.9		-0.09
704					1857	D7 0-12			
732					1881				
752					1906				
753					1949				
778					1986				
781					2129				
785 798					6054 6075				
823					6092				
824					6112				
825					6114				
840	D7042	713.89		-0.02	6201				
872					6238				
873					6262				
874 875					6298				
875 887					6340 6359	D7042	745.2		1.18
902					0008	D1 042	140.2		1.10
302					ı				

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normality	OK
n	17
outliers	1
mean (n)	714.2911
st.dev. (n)	13.43075
R(calc.)	37.6061
st.dev.(D7042:16e3)	26.25020
R(D7042:16e3)	73.5006





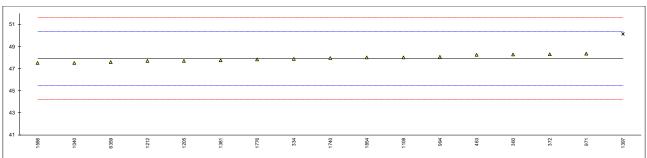
Fuel Oil: iis20F03 page 47 of 97

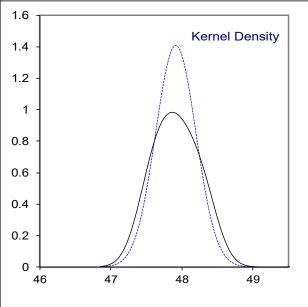
Determination of Viscosity Stabinger at 100°C on sample #20250; results in mm²/s

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904				
120					913				
140					914				
150 154					962 963				
159					971	D7042	48.36		0.36
168					974	D7042	40.30		0.30
169					994	D7042	48.06		0.12
170					995	D7 0-12			
171					996				
175					997				
212					1011				
225					1016				
230					1026				
237					1040	D7042	47.503		-0.34
238					1065				
253					1108	D7042	48.02		0.08
256					1109				
273					1121				
309 311					1126 1134				
313					1140				
323					1167				
333					1205	D7042	47.696		-0.18
334	D7042	47.87		-0.04	1212	D7042	47.688		-0.19
336	2.0.2				1213	2.0.2			
339					1277				
342					1299				
349					1320				
351					1356				
356					1367				
360	D7042	48.278		0.29	1381	D7042	47.759		-0.13
370	D7040				1397	D7042	50.14	G(0.01)	1.81
372	D7042	48.31		0.32	1402				
381 445					1510				
443					1556 1585				
463	D7042	48.239		0.26	1586	D7042	47.50		-0.34
495	D1042				1631	D7 0 12			
507					1635				
541					1648				
551					1650				
558					1681				
575					1720				
610					1724	D7040	47.05		
621					1740	D7042	47.95		0.03
631 633					1776 1792	D7042	47.832		-0.07
634					1792				
657					1854	D7042	48.0		0.07
704					1857	D7 0-12			
732					1881				
752					1906				
753					1949				
778					1986				
781					2129				
785					6054				
798					6075				
823					6092				
824 825					6112 6114				
825 840					6201				
872					6238				
873					6262				
874					6298				
875					6340				
887					6359	D7042	47.60		-0.26
902									

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normality	OK
n	16
outliers	1
mean (n)	47.9166
st.dev. (n)	0.28345
R(calc.)	0.7937
st.dev.(D7042:16e3)	1.22974
R(D7042:16e3)	3.4433





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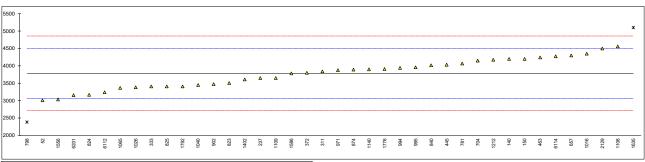
Determination of Nitrogen on sample #20250; results in mg/kg

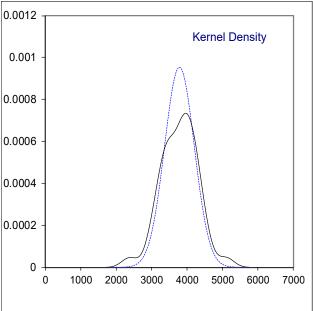
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4629	3000		-2.18	904				
120					913				
140	D5762 Volumetric	4200	С	1.16	914				
150	D5762 Volumetric	4200	· ·	1.16	962				
154	Boroz Volametro				963				
159					971	D5762 Gravimetric	3872		0.25
						D3762 Gravimetric			0.25
168					974	DE700 0 t t-i			0.40
169					994	D5762 Gravimetric	3938		0.43
170					995	D3228	3951		0.47
171					996				
175					997				
212					1011				
225					1016	D5762 Gravimetric	4345.12		1.57
230					1026	D5762 Volumetric	3380		-1.12
237	D4629	3642		-0.39	1040	D4629	3442		-0.95
238					1065	D5762 Gravimetric	3362		-1.17
253					1108	D5762 Gravimetric	4555		2.15
256					1109	D4629	3642		-0.39
273					1121	B 1020			
309					1126				
311	D5762 Volumetric	3834		0.14	1134				
	D3762 Volumetric					D4620			0.24
313					1140	D4629	3893.5231		0.31
323	D==001/1				1167				
333	D5762 Volumetric	3400		-1.06	1205				
334					1212	D3228	4170		1.08
336					1213				
339					1277				
342					1299				
349					1320				
351					1356				
356					1367				
360					1381				
370					1397				
372	D5762 Volumetric	3800		0.05	1402	D5762 Volumetric	3600		-0.51
381	Boroz Volamento				1510	DOTOL VOIGINIONIO			
445	D5762 Gravimetric	4030		0.69	1556	D5762 Volumetric	3028		-2.10
447	D3702 Gravimetric				1585	D3702 Volumetric			-2.10
	D5762 Gravimetric	4242		1.28	1586	D5762 Volumetric	3783		0.00
463	D3762 Gravimetric					D3762 Volumetric			0.00
495					1631	DE700 Carriage atain	 5400	D(0.05)	2.07
507					1635	D5762 Gravimetric	5100	R(0.05)	3.67
541					1648				
551					1650				
558					1681				
575					1720				
610					1724				
621					1740				
631					1776	D5762 Volumetric	3900.65		0.33
633					1792	D3228	3405		-1.05
634					1796				
657	D5762 Gravimetric	4300		1.44	1854				
704	D5762 Gravimetric	4146		1.01	1857				
732					1881				
752					1906				
753					1949				
778					1986				
781	D3228	4060		0.77	2129	D3228	4501		2.00
785	טטעעט	4000		0.77	6054	שטבבט	4301		2.00
	DETEC Crossing state		פיט סבי						
798	D5762 Gravine tric	2375	R(0.05)	-3.92	6075				
823	D5762 Gravimetric	3500		-0.78	6092	DE700 \ / \			4.50
824	D5762 Gravimetric	3163		-1.72	6112	D5762 Volumetric	3235		-1.52
825	D5762 Gravimetric	3400		-1.06	6114	D5762 Volumetric	4274		1.37
840	D3228	4010		0.63	6201	D5762 Gravimetric	3150		-1.76
872					6238				
873					6262				
874	D5762 Volumetric	3886		0.29	6298				
875					6340				
887					6359				
902	D5762 Gravimetric	3473		-0.86	1				

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normality	OK
n	38
outliers	2
mean (n)	3781.93
st.dev. (n)	418.328
R(calc.)	1171.32
st.dev.(D5762:18a)	359.283
R(D5762:18a)	1005.99

Lab 140 first reported 5100





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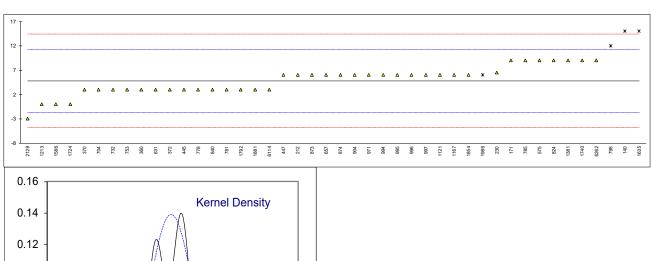
Determination of Pour Point, Lower on sample #20250; results in °C

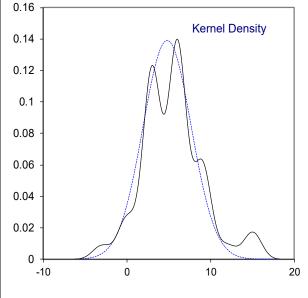
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52					904	ISO3016	6		0.37
120					913				
140	D97	15	R(0.05)	3.17	914				
150					962				
154					963	1000010			
159					971	ISO3016	6		0.37
168					974	D07			0.07
169 170					994	D97	6		0.37
170 171	ISO3016	9		1.30	995 996	ISO3016 D97	6 6		0.37 0.37
175	1303010				997	ISO3016	6		0.37
212	ISO3016	6		0.37	1011	1000010			
225	1000010				1016				
230	ISO3016	6.47		0.52	1026				
237					1040				
238					1065				
253					1108				
256					1109				
273					1121	ISO3016	6		0.37
309					1126				
311					1134				
313 323					1140 1167	ISO3016	6		0.37
333					1205	1303010	0		0.37
334					1212				
336					1213	D97	0		-1.50
339					1277	20.			
342					1299				
349					1320				
351					1356				
356					1367				
360	ISO3016	3		-0.56	1381	ISO3016	9.0		1.30
370	D97	3		-0.56	1397				
372	ISO3016	3		-0.56	1402				
381 445	D97			0.56	1510				
445 447	ISO3016	3 6		-0.56	1556				
463	1303010			0.37	1585 1586	D97	0		-1.50
495					1631	D31			-1.50
507					1635	ISO3016	15	R(0.05)	3.17
541					1648			()	
551					1650				
558					1681				
575	D97	9		1.30	1720				
610					1724	D97	0		-1.50
621	D07			0.50	1740	D97	9		1.30
631	D97	3		-0.56	1776	ISO3016	2		0.56
633 634					1792 1796	1303010	3		-0.56
657	ISO3016	6		0.37	1854	ISO3016	6		0.37
704	D97	3		-0.56	1857	1000010			
732	D97	3		-0.56	1881	ISO3016	3		-0.56
752					1906				
753	ISO3016	3		-0.56	1949				
778	ISO3016	3		-0.56	1986	ISO3016	6	ex	0.37
781	ISO3016	3		-0.56	2129	D97	-3		-2.43
785	ISO3016	9		1.30	6054				
798	D97	12	ex	2.24	6075				
823 824	ISO3016	9		1.30	6092 6112				
825	1000010	9 		1.30	6114	D97	3		-0.56
840	D97	3		-0.56	6201	וטטו	J 		-0.30
872	20.			-0.50	6238				
873	D97	6		0.37	6262	D97	9		1.30
874	ISO3016	6		0.37	6298				
875					6340				
887					6359				
902									

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normality	OK
n	40
outliers	2 (+2ex)
mean (n)	4.81
st.dev. (n)	2.872
R(calc.)	8.04
st.dev.(ISO3016:19)	3.214
R(ISO3016:19)	9

Lab 798 test result excluded as PP lower > PP upper, which is in principle not possible Lab 1968 test result excluded as PP lower > PP upper, which is in principle not possible





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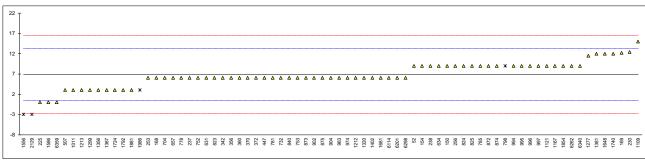
Determination of Pour Point, Upper on sample #20250; results in °C

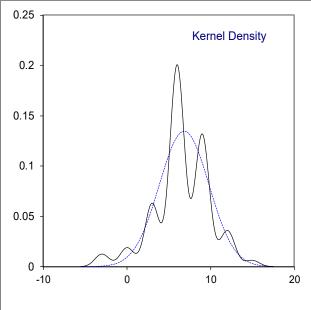
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D97	9		0.67	904	ISO3016	6		-0.26
120					913				
140					914				
	D07	0							
150	D97	9		0.67	962	1000040			0.00
154	D97	9		0.67	963	ISO3016	6		-0.26
159					971				
168	D97	6		-0.26	974	D97	6		-0.26
169	D97	12.2		1.67	994	D97	9		0.67
170					995	ISO3016	9		0.67
171					996	D97	9		0.67
175					997	ISO3016	9		0.67
212					1011	D97	3		-1.20
225	D97	0			1016	D31	3		-1.20
				-2.13					
230	ISO3016	12.41		1.73	1026				
237	D97	6		-0.26	1040				
238	D97	9		0.67	1065				
253	D97	6		-0.26	1108				
256	D97	9.0		0.67	1109	D97	15		2.54
273					1121	ISO3016	9		0.67
309					1126				
311					1134				
313					1140				
						1002016	9		0.67
323					1167	ISO3016			0.67
333					1205				
334					1212	ISO3016	6		-0.26
336					1213	D97	3		-1.20
339					1277	D97	11.5		1.45
342	ISO3016	6		-0.26	1299	D97	3		-1.20
349					1320	ISO3016	6		-0.26
351					1356	ISO3016	3		-1.20
356	ISO3016	6		-0.26	1367	D97	3		-1.20
360	ISO3016	6		-0.26	1381	ISO3016	12.0		1.60
370	D97	6		-0.26	1397				
372	ISO3016	6		-0.26	1402	ISO3016	6		-0.26
381					1510				
445					1556	ISO3016	-3.0	DG(0.05)	-3.06
447	ISO3016	6		-0.26	1585			, ,	
463					1586	D97	0		-2.13
495					1631	201			
507	ISO3016	3		-1.20	1635				
	1303010	3				1000040			
541					1648	ISO3016	12		1.60
551					1650				
558					1681	ISO3016	6		-0.26
575					1720				
610					1724	D97	3		-1.20
621					1740	D97	12		1.60
631	D97	6		-0.26	1776				
633					1792	ISO3016	3		-1.20
634	D97	9		0.67	1796	1000010			
657	ISO3016	6		-0.26	1854	1503016	9		0.67
						ISO3016			
704	D97	6		-0.26	1857	1000010			
732	D97	6		-0.26	1881	ISO3016	3		-1.20
752	D97	6		-0.26	1906				
753	ISO3016	6		-0.26	1949				
778	ISO3016	6		-0.26	1986	ISO3016	3	ex	-1.20
781	ISO3016	6		-0.26	2129	D97	-3	DG(0.05)	-3.06
785	ISO3016	9		0.67	6054			()	
798	D97	9	ex	0.67	6075				
			υ Λ						
823	ISO3016	6		-0.26	6092				
824	ISO3016	9		0.67	6112	D07			
825	ISO3016	9		0.67	6114	D97	6		-0.26
840	D97	6		-0.26	6201	D97	6		-0.26
872	ISO3016	9		0.67	6238				
873	D97	6		-0.26	6262	D97	9		0.67
874	ISO3016	9		0.67	6298	D97	6		-0.26
875	D97	6		-0.26	6340	D97	9		0.67
887					6359	D97	Ő		-2.13
902	ISO3016	6		-0.26	0000	201	U		-2.10
902	1303010	U		-0.20	I				

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normality	OK
n	71
outliers	2 (+2ex)
mean (n)	6.85
st.dev. (n)	2.969
R(calc.)	8.31
st.dev.(ISO3016:19)	3.214
R(ISO3016:19)	9

Lab 798 test result excluded as PP lower > PP upper, which is in principle not possible Lab 1968 test result excluded as PP lower > PP upper, which is in principle not possible





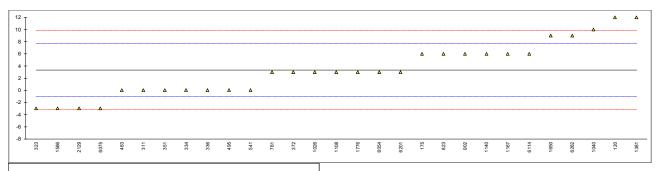
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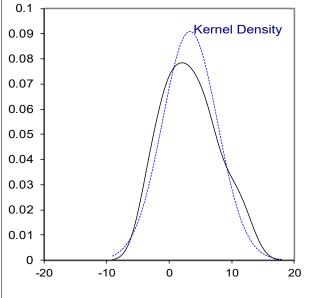
Determination of Pour Point, Automated, 3°C interval on sample #20250; results in °C

lab	method	value	mark	z(targ)	lab	method	value	mark z(targ)
52	DE040	40		2.07	904			
120 140	D5949	12		3.97	913 914			
150					962			
154					963			
159					971			
168					974			
169					994			
170					995			
171					996			
175	D5950	6.0		1.22	997			
212	50000				1011			
225					1016			
230					1026	D5950	3	-0.16
237					1040	ISO3016	10.0	3.05
238					1065			
253					1108	D5950	3	-0.16
256					1109			
273					1121			
309					1126			
311	D5950	0		-1.54	1134			
313					1140	D5950	6.0	1.22
323	D5950	-3		-2.91	1167	D6749	6	1.22
333					1205			
334	D5950	0		-1.54	1212			
336	D5950	0		-1.54	1213			
339					1277			
342					1299			
349					1320			
351	D6749	0.0		-1.54	1356			
356					1367			
360					1381	D6749	12.0	3.97
370					1397			
372	D5950	3		-0.16	1402			
381					1510			
445					1556			
447					1585			
463	D6892	0		-1.54	1586	D5950	-3.0	-2.91
495	D6892	0		-1.54	1631			
507	D5050			4.54	1635			
541	D5950	0		-1.54	1648	DEOEO		2.00
551 550					1650	D5950	9.0	2.60
558 575					1681 1720			
610					1724			
621					1724			
631					1776	D5950	3	-0.16
633					1792	D3930		-0.10
634					1796			
657					1854			
704					1857			
732					1881			
752					1906			
753					1949			
778					1986			
781	D5950	3		-0.16	2129	D5950	-3.0	-2.91
785					6054	D5950	3	-0.16
798					6075		-3	-2.91
823	D5950	6		1.22	6092			
824					6112			
825					6114	D5950	6	1.22
840					6201	D5950	3	-0.16
872					6238			
873					6262	D6892	9	2.60
874					6298			
875					6340			
887					6359			
902	D6892	6		1.22				

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normality	OK
n	29
outliers	0
mean (n)	3.34
st.dev. (n)	4.394
R(calc.)	12.30
st.dev.(D5950:14)	2.179
R(D5950:14)	6.1





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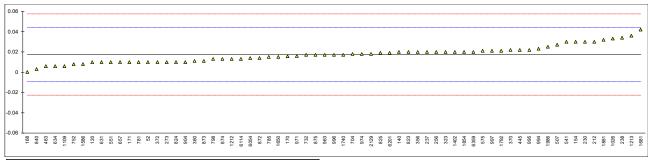
Determination of Sediment by Extraction on sample #20250; results in %M/M

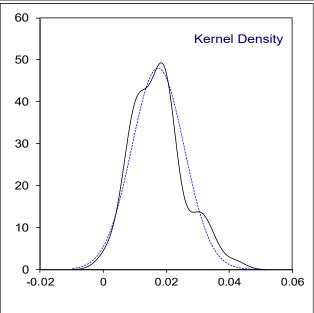
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D473	0.01	man	-0.56	904	ISO3735	0.01	mun	-0.56
120	D473	0.01		-0.56	913	1000700			
140	D473	0.02		0.19	914				
150	D+13				962				
154	D473	0.03		0.94	963	D473	0.017		-0.03
159	D+10				971	D473	0.016		-0.03
168	D473	0.00		-1.30	974	D473	0.018		0.04
169	D473			-1.50	994	D473	0.013		0.42
170	D473	0.0155		-0.14	995	D473 D473	0.023		0.42
170	D473	0.0155			996	D473 D473	0.022		
	D473			-0.56					-0.03
175 212	D473	0.03		0.94	997 1011	D473	0.021		0.27
212	D473				1011				
230	D473	0.03	С	0.94	1016	D473	0.033	С	1.16
237	D473	0.03	C	0.94	1020	D473		C	
238	D473	0.02		1.24	1040				
	D473								
253 256	D473	0.02		0.19	1108	D473	0.006		-0.86
					1109	D473	0.000		-0.00
273 309	D473	0.01		-0.56	1121 1126				
311					1134				
313	D472	0.00		0.40	1140				
323	D473	0.02		0.19	1167				
333					1205	D472	0.012		0.22
334					1212	D473	0.013		-0.33
336					1213	D473	0.036		1.39
339					1277				
342					1299				
349					1320				
351	D472	0.00		0.40	1356				
356	D473	0.02		0.19	1367				
360	D473	0.011		-0.48	1381				
370	D473	0.022		0.34	1397	IDEO	0.00		0.40
372	D473	0.01		-0.56	1402	IP53	0.02		0.19
381	D.470			0.04	1510				
445	D473	0.022		0.34	1556				
447	D.470				1585	D 470			0.74
463	D473	0.006		-0.86	1586	D473	0.0080		-0.71
495	D.470	0.007		0.70	1631				
507	D473	0.027		0.72	1635				
541	D473	0.030		0.94	1648	D. 170			
551	D473	0.01		-0.56	1650	D473	0.015		-0.18
558	D.170				1681	D473	0.042		1.84
575	D473	0.021		0.27	1720				
610					1724	D.170			
621	D.170				1740	D473	0.017		-0.03
631	D473	0.010		-0.56	1776	D.170			
633	D.470				1792	D473	0.021		0.27
634	D473	0.006		-0.86	1796	D 470			
657	D473	0.01		-0.56	1854	D473	0.020		0.19
704	D473	0.018		0.04	1857	D 470			4.00
732	D473	0.017		-0.03	1881	D473	0.032		1.09
752	ISO3735	0.008		-0.71	1906				
753					1949	10.00705			
778	D.170				1986	ISO3735	0.025		0.57
781	D473	0.01		-0.56	2129	IP53	0.018		0.04
785	D473	0.015		-0.18	6054	D473	0.01381		-0.27
798	D473	0.013		-0.33	6075				
823	D473	0.02		0.19	6092				
824	D473	0.01		-0.56	6112	D.470			
825	D473	0.0189		0.11	6114	D473	0.013		-0.33
840	D473	0.003		-1.08	6201	D473	0.019		0.12
872	D473	0.014		-0.26	6238				
873	D473	0.011		-0.48	6262				
874	D473	0.013		-0.33	6298				
875	D473	0.017		-0.03	6340	B.1=0			
887					6359	D473	0.02		0.19
902					l				

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normality	OK
n	67
outliers	0
mean (n)	0.0174
st.dev. (n)	0.00830
R(calc.)	0.0232
st.dev.(D473:07e1)	0.01337
R(D473:07e1)	0.0374

Lab 230 first reported 1.84 Lab 1026 first reported 0.074





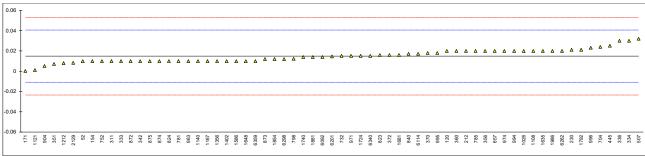
Fuel Oil: iis20F03 page 59 of 97

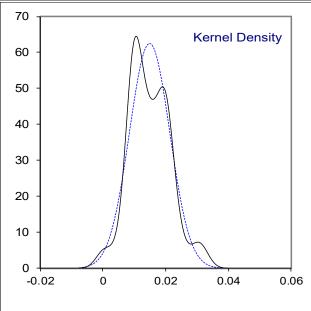
Determination of Total Sediment Existent (TSE) of sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value mark	z(targ)
52	D4870	0.01		-0.38	904	IP375	0.005	-0.77
120	D4870	0.02		0.40	913			
140					914			
150					962			
154	D4870	0.01		-0.38	963	IP375	0.01	-0.38
159	2.0.0				971	ISO10307-1	0.015	0.01
168					974	IP375	0.02	0.40
169					994	IP375	0.020	0.40
170					995	IP375	0.018	0.24
170	IP375	0.00		-1.16	996	D4870	0.023	0.63
175	11 37 3			-1.10	997	D4070	0.023	0.03
212	ISO10307-1	0.02		0.40	1011			
	130 10307-1	0.02						
225	10010207 1			0.48	1016	IP375	0.02	0.40
230	ISO10307-1	0.021			1026			0.40
237					1040	ISO10307-1	<0,01	
238					1065	10040007.4		
253					1108	ISO10307-1	0.02	0.40
256					1109			
273					1121	ISO10307-1	0.001	-1.08
309					1126			
311	ISO10307-1	0.01		-0.38	1134			
313					1140	IP375	0.01	-0.38
323					1167	ISO10307-1	0.01	-0.38
333	ISO10307-1	0.01		-0.38	1205			
334	IP375	0.03		1.18	1212	IP375	0.0078	-0.55
336	IP375	0.03		1.18	1213			
339					1277			
342	ISO10307-1	0.01		-0.38	1299	ISO10307-1	<0.01	
349					1320			
351	ISO10307-1	0.007		-0.62	1356	ISO10307-1	0.01	-0.38
356	IP375	0.02		0.40	1367	IP375	<0.01	
360	IP375	0.020		0.40	1381			
370	ISO10307-1	0.018		0.24	1397			
372	IP375	0.016		0.09	1402	IP375	0.01	-0.38
381	11 070				1510	IP375	<0.01	
445	IP375	0.025		0.79	1556	11 07 0		
447	11 373	0.025			1585			
463					1586	IP375	0.01	-0.38
495					1631	IF3/3	0.01	-0.36
	ID275	0.022		1 2 4		D4970		
507	IP375	0.032		1.34	1635	D4870	0.02	0.40
541	D4870	<0.01			1648	ISO10307-1	0.010	-0.38
551					1650	10040007.4		
558					1681	ISO10307-1	0.016	0.09
575					1720			
610					1724	IP375	0.015	0.01
621					1740	D4870	0.014	-0.07
631	D4870	<0.01			1776			
633					1792	IP375	0.021	0.48
634					1796			
657	IP375	0.02		0.40	1854	ISO10307-1	0.012	-0.23
704	IP375	0.024		0.71	1857			
732	D4870	0.015		0.01	1881	D4870	0.014	-0.07
752	ISO10307-1	0.010		-0.38	1906			
753					1949			
778					1986	ISO10307-1	0.02	0.40
781	IP375	0.01		-0.38	2129	IP375	0.00825	-0.52
785	IP375	0.02		0.40	6054	010		
798	IP375	0.0121		-0.22	6075			
823	ISO10307-1	0.0121		0.09	6092	IP375	0.014	-0.07
824	ISO10307-1	0.010		-0.38	6112	11 373	0.014	-0.07
	150 10507-1					10010207 1		
825 840	ISO10207 1	0.017		0.16	6114	ISO10307-1	0.017	0.16 -0.03
	ISO10307-1				6201	ISO10307-1	0.0145	-0.03
872	IP375	0.01		-0.38	6238	10010207 4	0.02	0.40
873	IP375	0.012		-0.23	6262	ISO10307-1	0.02	0.40
874	IP375	0.01		-0.38	6298	IP375	0.012	-0.23
875	IP375	0.01		-0.38	6340	IP375	0.015	0.01
887	100100-				6359	ISO10307-1	0.01	-0.38
902	ISO10307-1	<0,01			1			

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normality	OK
n	65
outliers	0
mean (n)	0.0149
st.dev. (n)	0.00638
R(calc.)	0.0179
st.dev.(IP375:11)	0.01281
R(IP375:11)	0.0359





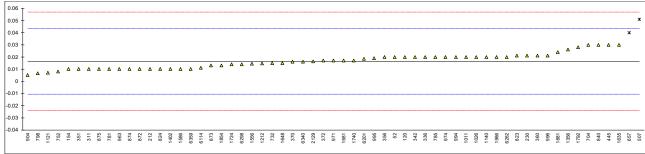
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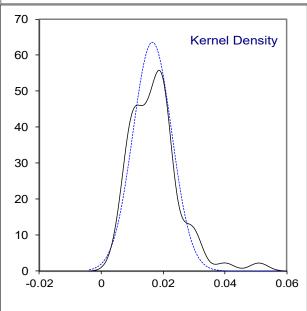
Determination of Total Sediment Accelerated (TSA) of sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value mar	k z(targ)
52	D4870	0.02	man	0.26	904	IP390	0.005	-0.86
120	D4870	0.02		0.26	913	11 000	0.000	-0.00
140	D4070				914			
150					962			
154	D4870	0.01		-0.49	963	IP390	0.01	-0.49
	D4070							
159					971	ISO10307-2	0.017	0.03
168					974	IP390	0.02	0.26
169					994	IP390	0.020	0.26
170	IDOOO				995	IP390	0.019	0.18
171	IP390	<0.01			996	D4870	0.021	0.33
175	100400-0				997	1001000		
212	ISO10307-2	0.01		-0.49	1011	ISO10307-2	0.02	0.26
225					1016			
230	ISO10307-2	0.021		0.33	1026	ISO10307-2	0.02	0.26
237					1040	ISO10307-2	<0,01	
238					1065			
253					1108			
256					1109			
273					1121	ISO10307-2	0.007	-0.71
309					1126			
311	ISO10307-2	0.01		-0.49	1134			
313					1140	IP390	0.02	0.26
323					1167	000		
333					1205			
334					1212	IP390	0.0146	-0.14
336	IP390	0.02		0.26	1213	11 330	0.0140	-0.14
339	11-390	0.02			1277			
	10040007.0			0.00		10040007.0		
342	ISO10307-2	0.02		0.26	1299	ISO10307-2	<0.01	
349	10040007.0			0.40	1320	10040007.0		0.70
351	ISO10307-2	0.010		-0.49	1356	ISO10307-2	0.026	0.70
356	IP390	0.02		0.26	1367	IP390	<0.01	
360	IP390	0.021		0.33	1381			
370	ISO10307-2	0.016		-0.04	1397			
372	IP390	0.017		0.03	1402	IP390	0.01	-0.49
381					1510			
445	IP390	0.03		1.00	1556	ISO10307-2	0.0145	-0.15
447					1585			
463					1586	IP390	0.01	-0.49
495					1631			
507	IP390	0.051	R(0.01)	2.55	1635	D4870	0.03	1.00
541					1648	ISO10307-2	0.015	-0.11
551					1650			
558					1681	ISO10307-2	0.017	0.03
575					1720			
610					1724	IP390	0.014	-0.19
621					1740	D4870	0.017	0.03
631	D4870	<0.01			1776			
633	2 .0.0				1792	IP390	0.028	0.85
634					1796	11 000		
657	IP390	0.04	R(0.05)	1.74	1854	ISO10307-2	0.013	-0.26
704	IP390	0.030	11(0.00)	1.00	1857	10010001-2	0.010	-0.20
732	D4870	0.030		-0.11	1881	IP390	0.024	0.55
752 752	ISO10307-2					15390		0.55
	13010307-2	0.008		-0.63	1906			
753 770					1949	10040007.0		0.00
778	IDOOO				1986	ISO10307-2	0.02	0.26
781	IP390	0.01		-0.49	2129	IP390	0.0164	-0.01
785	IP390	0.02		0.26	6054			
798	IP390	0.0066		-0.74	6075			
823	ISO10307-2	0.021		0.33	6092			
824	ISO10307-2	0.01		-0.49	6112			
825					6114	ISO10307-2	0.011	-0.41
840	ISO10307-2	0.030		1.00	6201	ISO10307-2	0.0185	0.14
872	IP390	0.01		-0.49	6238			
873	IP390	0.013		-0.26	6262	ISO10307-2	0.02	0.26
874	IP390	0.01		-0.49	6298	IP390	0.014	-0.19
875	IP390	0.01		-0.49	6340	IP390	0.016	-0.04
887					6359	ISO10307-2	0.01	-0.49
902	ISO10307-2	<0,01				- 	*******	00
	<u>-</u>	-,•.			1			

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OK
59
2
0.0166
0.00627
0.0176
0.01351
0.0378





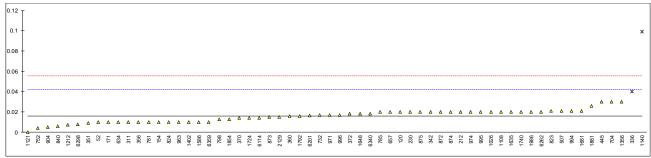
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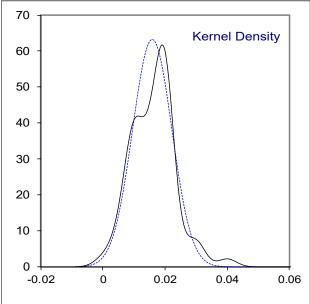
Determination of Total Sediment Potential (TSP) of sample #20250; results in %M/M

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4870	0.01	IIIaik	-0.44	904	IP390	0.005	IIIaik	-0.82
120	D4870	0.02		0.31	913	IF 390			-0.02
140	D4070	0.02		0.31	913				
150					962				
154	D4870	0.01		-0.44	963	IP390	0.01		-0.44
159	D4070			-0.44	971	ISO10307-2	0.017		0.09
168					974	IP390	0.02		0.09
169					994	IP390	0.021		0.31
170					995	IP390	0.021		0.33
170	IP390	0.01		-0.44	996	D4870	0.017		0.09
175	11 000			-0.44	997	D4070			0.03
212	ISO10307-2	0.02		0.31	1011				
225	10010001 2				1016				
230	ISO10307-2	0.020		0.31	1026	ISO10307-2	0.02		0.31
237					1040				
238					1065				
253					1108	ISO10307-2	0.02		0.31
256					1109				
273					1121	ISO10307-2	0.000		-1.20
309					1126				
311	ISO10307-2	0.01		-0.44	1134				
313					1140	IP390	0.099	R(0.01)	6.29
323					1167			, ,	
333					1205				
334					1212	IP390	0.0074		-0.64
336	IP390	0.04	R(0.05)	1.83	1213				
339					1277				
342	ISO10307-2	0.02		0.31	1299	ISO10307-2	<0.01		
349					1320				
351	ISO10307-2	0.009		-0.52	1356	ISO10307-2	0.03		1.07
356	IP390	0.01		-0.44	1367	IP390	<0.01		
360	IP390	0.016		0.01	1381				
370	ISO10307-2	0.014		-0.14	1397	ID000			
372	IP390	0.018		0.16	1402	IP390	0.01		-0.44
381	IDOOO				1510				
445	IP390	0.03		1.07	1556				
447 463					1585 1586	ISO10307-2	0.01		-0.44
495					1631	130 10307-2	0.01		-0.44
507	IP390	0.021		0.39	1635	D4870	0.02		0.31
541	11 000				1648	ISO10307-2	0.018		0.16
551					1650	10010007-2			
558					1681	ISO10307-2	0.021		0.39
575					1720	10010001 2			
610					1724	IP390	0.014		-0.14
621					1740	D4870	0.020		0.31
631	D4870	< 0.01			1776				
633					1792	IP390	0.016		0.01
634	D4870	0.01		-0.44	1796				
657	IP390	0.02		0.31	1854	ISO10307-2	0.013		-0.22
704	IP390	0.030		1.07	1857				
732	D4870	0.017		0.09	1881	IP390	0.026		0.77
752	ISO10307-2	0.004		-0.90	1906				
753					1949				
778					1986	ISO10307-2	0.02		0.31
781	IP390	0.01		-0.44	2129	IP390	0.015		-0.06
785	IP390	0.02		0.31	6054				
798	IP390	0.0129		-0.22	6075				
823	ISO10307-2	0.021		0.39	6092				
824	ISO10307-2	0.01		-0.44	6112	10040007.0			
825	10040007.0	0.006		0.74	6114	ISO10307-2	0.014		-0.14
840	ISO10307-2	0.006		-0.74	6201	ISO10307-2	0.0165		0.05
872	IP390	0.02		0.31	6238	10010207.0	0.02		0.21
873 874	IP390 IP390	0.015		-0.06	6262	ISO10307-2	0.02		0.31
	IP390 IP390	0.020 0.02		0.31	6298 6340	IP390 IP390	0.008		-0.59 0.16
875 887	11-220	0.02		0.31	6359	ISO10307-2	0.018 0.01		-0.44
902	ISO10307-2	<0,01			0359	130 10307-2	0.01		-0.44
302	100 10001-2	١ ٥,٥٠			I				

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normality	OK
n	60
outliers	2
mean (n)	0.0158
st.dev. (n)	0.00631
R(calc.)	0.0177
st.dev.(IP390:11)	0.01322
R(IP390:11)	0.0370





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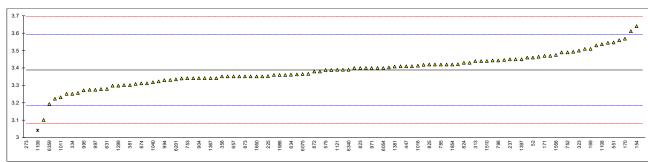
Determination of Total Sulfur on sample #20250; results in %M/M

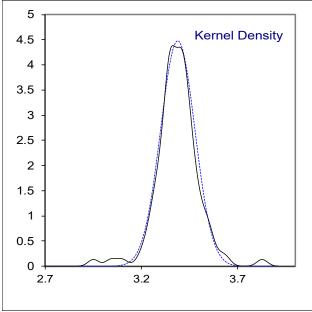
lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D4294	3.46	IIIdik	0.70	904	ISO8754	3.34	mark	-0.47
	D4294			2.17	913	1300734			-0.47
120	D4294 D4294	3.61128			913				
140		3.42		0.31					
150	D4294	3.56		1.67	962	1000754	2.40		0.44
154	D4294	3.64		2.45	963	ISO8754	3.40		0.11
159	D 400 4				971	ISO8754	3.40		0.11
168	D4294	3.53		1.38	974	D4294	3.39		0.02
169	D4294	3.51		1.19	994	D4294	3.329		-0.58
170	D4294	3.5682		1.75	995	ISO8754	3.271		-1.14
171	D4294	3.47		0.80	996	D4294	3.256		-1.29
175	D4294	3.51		1.19	997	ISO8754	3.274		-1.11
212	ISO8754	3.44		0.50	1011	ISO8754	3.23		-1.54
225	D4294	3.352		-0.35	1016	ISO8754	3.412		0.23
230	D4294	3.297		-0.89	1026	D2622	3.418		0.29
237	D4294	3.45		0.60	1040	ISO8754	3.317		-0.69
238	D4294	3.274		-1.11	1065	D4294	3.34		-0.47
253	D4294	3.40		0.11	1108	ISO8754	3.536		1.44
256					1109	D4294	3.04	R(0.05)	-3.39
273	D4294	2.5	C,R(0.01)	-8.66	1121	ISO8754	3.3895		0.01
309	D4294	3.493	С	1.02	1126				
311	ISO8754	3.46		0.70	1134				
313	ISO8754	3.44		0.50	1140	IP336	3.465		0.75
323	ISO8754	3.50		1.09	1167				
333	ISO8754	3.10		-2.81	1205				
334	ISO8754	3.25		-1.35	1212	ISO8754	3.45		0.60
336					1213	D4294	3.827	C,R(0.01)	4.28
339	INH-050	3.49		0.99	1277	D4294	2.95	R(0.01)	-4.27
342	ISO8754	3.442		0.52	1299	D2622	3.297	, ,	-0.89
349					1320				
351	ISO8754	3.402		0.13	1356	ISO8754	3.35		-0.37
356	ISO8754	3.35		-0.37	1367	IP336	3.34		-0.47
360	ISO8754	3.30		-0.86	1381	ISO8754	3.407		0.18
370	ISO8754	3.366		-0.22	1397	D2622	3.45		0.60
372	ISO8754	3.42		0.31	1402	IP336	3.33		-0.57
381	ISO8754	3.3		-0.86	1510	ISO8754	3.44		0.50
445	IP336	3.544		1.52	1556	ISO8754	3.4747		0.84
447	IP336	3.41		0.21	1585				
463	ISO8754	3.35		-0.37	1586	ISO8754	3.277		-1.08
495	ISO8754	3.222		-1.62	1631	1000701			
507	ISO8754	3.341		-0.46	1635	D4294	3.36		-0.28
541	1000101				1648	ISO8754	3.421		0.32
551	D4294	3.5463		1.54	1650	ISO8754	3.35		-0.37
558	D-120-1				1681	ISO8754	3.339		-0.48
575	D4294	3.3876		-0.01	1720	1000104			
610	D7237			-0.01	1724	IP336	3.31		-0.76
621					1740	D4294	3.40		0.11
631	D4294	3.279		-1.06	1776	ISO8754	3.410		0.11
633	D4294	J.27 9		-1.00	1792	ISO8754	3.307		-0.79
634	D4294	3.361		-0.27	1796	1300734	3.307		-0.79
657	D4294	3.35		-0.27	1854	ISO8754	3.42		0.31
704	ISO8754	3.350		-0.37	1857	1300734	J.42 		0.51
732	ISO8754	3.323		-0.57 -0.64	1881	ISO8754	3.35		-0.37
752 752	D4294	3.49		0.99		D5623		С	
					1906 1949	D3023	3.409	C	0.20
753 770	ISO8754	3.34		-0.47		1000754	2.26		0.20
778	D4294	3.47		0.80	1986	ISO8754	3.36		-0.28
781 705	ISO8754	3.446		0.56	2129	D4294	3.362		-0.26
785	ISO8754	3.42		0.31	6054	D4294	3.40		0.11
798	D4294	3.443		0.53	6075	ISO8754	3.365		-0.23
823	ISO8754	3.40		0.11	6092	D4294	3.43		0.41
824	ISO8754	3.43		0.41	6112	D 400 4			
825	ISO8754	3.42		0.31	6114	D4294	3.388		0.00
840	D4294	3.250		-1.35	6201	ISO8754	3.334		-0.53
872	ISO8754	3.38		-0.08	6238				
873	D4294	3.35		-0.37	6262	D 400 f			
874	D4294	3.31		-0.76	6298	D4294	3.36		-0.28
875	D4294	3.38		-0.08	6340	D4294	3.39		0.02
887	1000==:				6359	D2622	3.1918		-1.91
902	ISO8754	3.34		-0.47					

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OK
104
4
3.3883
0.08913
0.2496
0.10261
0.2873
0.1596

Lab 273 first reported 3.0 Lab 309 first reported 3.07 Lab 1213 first reported 0.827 Lab 1906 first reported 2.912





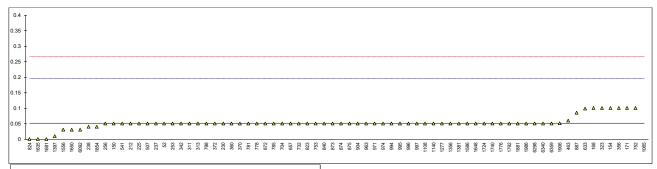
Fuel Oil: iis20F03 page 67 of 97

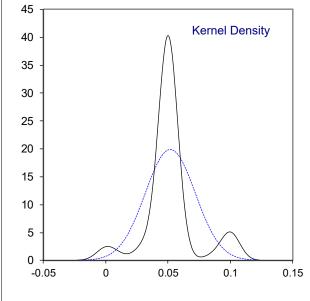
Determination of Water by distillation on sample #20250; results in %V/V

lab	method	value	mark	z(targ)	lab	method	value	mark	z(targ)
52	D95	0.05	mark	-0.02	904	ISO3733	0.05	IIIQIK	-0.02
120	D95	<0.05		-0.02	913	1000700			-0.02
140	Dao				914				
	DOE								
150	D95	0.05		-0.02	962	1000700	0.05		0.00
154	D95	0.10		0.68	963	ISO3733	0.05		-0.02
159	505				971	ISO3733	0.05		-0.02
168	D95	0.10		0.68	974	D95	0.05		-0.02
169					994	D95	0.05		-0.02
170					995	ISO3733	0.05		-0.02
171	D95	0.10		0.68	996	D95	0.05		-0.02
175					997	ISO3733	0.05		-0.02
212	ISO3733	0.05		-0.02	1011	ISO3733	<0.10		
225	D95	0.05		-0.02	1016				
230	ISO3733	0.05		-0.02	1026	D95	<0.025		
237	D95	0.05		-0.02	1040				
238	D95	0.04		-0.16	1065	D6304-A	1.1863	R(0.01)	15.88
253	D95	0.05		-0.02	1108	ISO3733	0.05	, ,	-0.02
256	D95	0.05		-0.02	1109	D95	< 0.025		
273	D95	< 0.05			1121	ISO3733	<0.05		
309	200				1126				
311	D95	0.05		-0.02	1134				
313	D95	0.05		-0.02	1140	IP74	0.05		-0.02
323	ISO3733	0.10		0.68	1167	EN1428	<0.1		-0.02
333	D95	<0.1			1205	LIN 1420			
334	D95	<0.1			1212				
						DOF			
336	ISO3733	<0.10			1213	D95	<0.1		0.00
339	1000700				1277	D95	0.05		-0.02
342	ISO3733	0.05		-0.02	1299	D95	<0.1		
349	D95	<0,1			1320	500011			
351	ISO3733	<0,05			1356	D6304-A	0.05		-0.02
356	ISO3733	0.10		0.68	1367	D95	<0.05		
360	ISO3733	0.05		-0.02	1381	ISO3733	0.05		-0.02
370	D95	0.05		-0.02	1397	ISO3733	0.01		-0.58
372	ISO3733	0.05		-0.02	1402	IP74	<0.05		
381					1510	ISO3733	<0.05		
445	D95	< 0.05			1556	D6304-C	0.03		-0.30
447	D95	<0.10			1585				
463	ISO3733	0.06		0.12	1586	D95	0.05		-0.02
495					1631				
507	ISO3733	0.050		-0.02	1635	D95	0.00		-0.72
541	D95	0.05		-0.02	1648	ISO3733	0.05		-0.02
551	D95	< 0.05			1650	D95	0.03		-0.30
558					1681	ISO3733	0.0		-0.72
575	D95	< 0.05			1720				
610					1724	D95	0.05		-0.02
621					1740	D95	0.05		-0.02
631	D95	< 0.01			1776	D6304-A	0.05		-0.02
633	D95	0.098		0.65	1792	ISO3733	0.05		-0.02
634	D95	< 0.05			1796				
657	D95	0.05		-0.02	1854	ISO3733	0.04		-0.16
704	ISO3733	0.05		-0.02	1857				
732	D95	0.05		-0.02	1881	D95	0.05		-0.02
752	D95	0.10		0.68	1906	D6304-C	0.051		-0.01
753	ISO3733	0.05		-0.02	1949				
778	D95	0.05		-0.02	1986	ISO3733	0.05		-0.02
781	ISO3733	0.05		-0.02	2129	D95	<0.05		
785	D95	0.05		-0.02	6054	D95	< 0.05		
798	D95	0.05		-0.02	6075	Воо			
823	ISO3733	0.05		-0.02	6092	D95	0.03		-0.30
824	ISO3733	0.05		-0.02 -0.72	6112	טפט	0.03		-0.30
825	ISO3733			-0.72		D95	< 0.05		
840		L0.05		-0.02	6114		<0.05		
	D95	0.05			6201	D95			
872 873	ISO3733	0.05		-0.02	6238	DOF	 <0.05		
873	D95	0.05		-0.02	6262	D95	<0,05		0.00
874	D95	0.05		-0.02	6298	D95	0.05		-0.02
875	D95	0.05		-0.02	6340	D95	0.05		-0.02
887	D95	0.085		0.47	6359	D95	0.05		-0.02
902	ISO3733	<0,1							

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normality n outliers mean (n) st.dev. (n) R(calc.) st.dev.(ISO3733:99)	not OK 73 1 0.0517 0.02004 0.0561 0.07143
R(ISO3733:99)	0.2
Compare	
. R(D95:13)	0.2





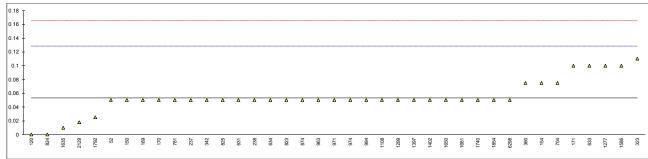
Fuel Oil: iis20F03 page 69 of 97

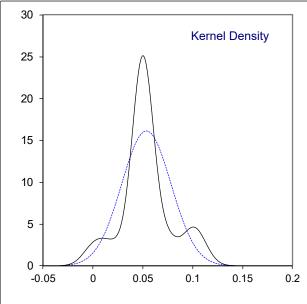
Determination of Water and Sediment on sample #20250; results in %V/V

lab	method	value	mark z(targ)	lab	method	value mark	z(targ)
52	D1796	0.05	-0.09	904			
120	D1796	0.00	-1.43	913			
140	21100			914			
150	D1796	0.05	-0.09	962			
154	D1796	0.03	0.57	963	D1796	0.05	-0.09
	D1790						
159				971	D1796	0.05	-0.09
168	D.1=00			974	D1796	0.05	-0.09
169	D1796	0.05	-0.09	994	D1796	0.05	-0.09
170	D1796	0.050	-0.09	995			
171	D1796	0.10	1.24	996			
175				997			
212				1011			
225				1016			
230				1026			
237	D1796	0.05	-0.09	1040			
238	D1796	0.05	-0.09	1065			
253				1108	D1796	0.05	-0.09
256				1109	D1796	<0.05	
273				1121	D1700		
309				1126			
311				1134			
313	D4700	0.44		1140			
323	D1796	0.11	1.51	1167			
333				1205			
334				1212			
336				1213			
339				1277	D1796	0.1	1.24
342	D1796	0.05	-0.09	1299	D1796	0.05	-0.09
349				1320			
351				1356			
356				1367			
360	D1796	0.075	0.57	1381			
370				1397	ISO3734	0.05	-0.09
372				1402	D1796	0.05	-0.09
381				1510	200		
445				1556			
447				1585			
463				1586	D1796	0.10	1.24
495				1631	D1730		1.24
507					D1796	0.01	
	D4700			1635	D1790		-1.16
541	D1796	<0.1		1648	D4700		0.00
551				1650	D1796	0.05	-0.09
558				1681	D1796	0.05	-0.09
575				1720			
610				1724			
621				1740	D1796	0.05	-0.09
631	D1796	0.05	-0.09	1776			
633	D1796	0.1	1.24	1792	D1796	0.025	-0.76
634	D1796	0.05	-0.09	1796			
657	D1796	<0.05		1854	D1796	0.05	-0.09
704	D1796	0.075	0.57	1857			
732				1881			
752				1906			
753				1949			
778				1986			
781	D1796	0.05	-0.09	2129	Calculation	0.018	-0.95
785				6054			
798				6075			
823	ISO3734	0.05	-0.09	6092			
824	D1796	0.00	-1.43	6112			
825	D1796	0.05	-0.09	6114			
840	71100	0.05	-0.09	6201		_ 	
872				6238			
873							
	D1706			6262	D1706	0.05	0.00
874 975	D1796	0.05	-0.09	6298	D1796	0.05	-0.09
875				6340			
887				6359			
902				I			

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normality	suspect
n	39
outliers	0
mean (n)	0.0535
st.dev. (n)	0.02473
R(calc.)	0.0692
st.dev.(D1796:11)	0.03750
R(D1796:11)	0.1050





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Vacuum Distillation at 10 mmHg but reported as AET on sample #20250, results in °C

lab	method	IBP	5%rec	10%rec	20%rec	30%rec	40%rec	50%rec	FBP
52									
120 140									
150	D1160	199	288	338	402	456	496	526	537
154									
159									
168 169									
170									
171	D1160	194	222 (R1)	334	403	457	496	525	525
175 212									
225									
230									
237 238									
253									
256									
273									
309 311									
313									
323									
333 334									
336									
339									
342 349									
351									
356	D1160	189	280	328	401	455	494	524	530
360	D1160	222	301	344	409	464	501		520
370 372	D1160	192	280	325	395	453	489	525	530
381	51100								
445	D1160	176.1	272.1	318.1	389.9	449.2	488.9	518.2	522.0
447 463	D1160	217	293	350	 427 (R1)	484 (R1)			502
495	D1100								
507									
541 551									
558									
575									
610									
621 631									
633									
634	D4400	400				45.4	400		
657 704	D1160 D1160	192 185.0	280 271.0	327 323.0	398 394.0	454 450.0	492 491.0	520 520.0	527 526.0
732	D1160	182.7	270.8	327.9	394.5	453	492.6	523.7	530
752	D1160	185	277	327	397	458	495	522	522
753 778									
781	D1160	182	265	316	391	449	493		514
785	D1160	192	281	324	400	458	502		524
798 823									
824									
825									
840	D1160	102	272	225	201	440	404		 510
872 873	D1160 D1160	193 185	273 272	325 322	391 394	449 450	494 494		519 518
874	D1160	185	271	322	395	450	493		518
875	D1160	188	268	322	397	452	501		520
887 902									
904									
913									
914 962									
962	D1160	181.4	273.2	318.9	385.6	442.4	481.1		522.4 C
971	D1160	203.1	281.2	326.4	397.2	454.2	495.2	525.1	528.6
974									

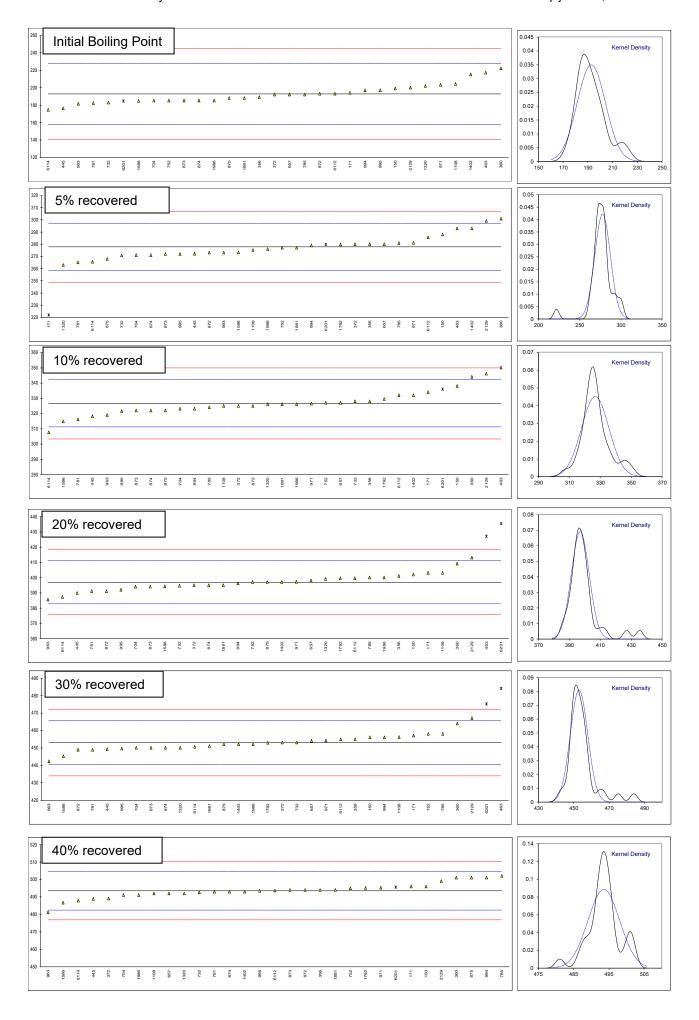
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lab	method	IBP	5%rec	10%rec	20%rec	30%rec	40%rec	50%rec	FBP
994	D1160	197.0	279.0	323.0	396.0	456.0	501.0	529.0	536.0
995	D1160	197.0	272.0	321.5	392.0	449.5	493.5	523.5	531.5
996									
997									
1011									
1016 1026									
1040									
1065									
1108	D1160	204.2	275.3	324.9	403.0	456.2	491.9	522.2	530.4
1109									
1121									
1126									
1134									
1140									
1167									
1205 1212									
1213									
1277									
1299									
1320	D1160	202	263	326	399	450	492	523	526
1356									
1367									
1381									
1397 1402		215	293	332	397	452	493	525	530
1510			293		391 	432	493	J2J 	
1556									
1585									
1586	D1160	184.9	273.4	314.7	394.2	445.2	486.7	517.7	517.7
1631									
1635									
1648									
1650 1681									
1720									
1724									
1740									
1776									
1792			279.8	329.4	399.4	452.9	495.1	527.3	528.6
1796									
1854									
1857 1881	D1160	188	277	326	395	451	494	 526	531
1906	ווט			320		451	494	526 	
1949									
1986		185	276	326	400	452	491	522	527
2129	D1160	200	299	346	413	467	499		
6054									
6075									
6092	D4400	400.0				454.0	400.0	 504.4	504.4
6112 6114	D1160 D1160	193.0 174.4	285.5 265.6	331.9 307.6	399.4 387.2	454.8 450.5	493.6 487.8	521.1 506.9 (R1)	521.1 508
6201	D1160	184.3 ex	279.7 ex	335.8 ex	435.4 (R1)	475.2 (R1)	495.6 ex	540.4 (R1)	551.3 (R5)
6238	51100								
6262			W	W	W	W	W	W	W
6298									
6340									
6359		W	W	W	W	W	W	W	W
	normality	ОК	OK	ellencot	cuencot	ellepoct	elichoot	OK	elleboot
	n	30	30	suspect 31	suspect 30	suspect 30	suspect 30	OK 20	suspect 30
	outliers	0 (+1ex)	1 (+1ex)	0 (+1ex)	2	2	0 (+1ex)	2	1
	mean (n)	192.79	277.86	326.69	396.98	453.03	493.58	523.29	524.08
	st.dev. (n)	11.408	9.465	8.866	5.772	4.920	4.500	2.941	7.656
	R(calc.)	31.94	26.50	24.82	16.16	13.78	12.60	8.23	21.44
	st.dev.(D1160:18)	17.500	9.605	7.757	7.064	6.330	5.557	5.189	9.643
	R(D1160:18)	49	26.89	21.72	19.78	17.72	15.56	14.53	27

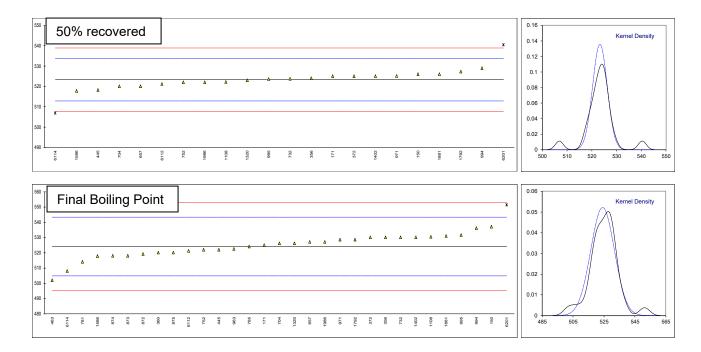
R1 and R5 respectively outlier and straggler in Rosner's outlier test

Lab 963 first reported 491.5 Lab 6262 test result withdrawn, reported 292.9, 333.2, 397.0, 452.4, 498.1, 535.6, 563.6 Lab 6359 test result withdrawn, reported 225, 249.3, 267.9, 300.7, 363.1, 478.9, 479.6, 480

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z-scores of Vacuum Distillation at 10 mmHg but reported as AET on sample #20250

lab	IBP	5%rec	10%rec	20%rec	30%rec	40%rec	50%rec	FBP
52								
120 140								
150	0.35	1.06	1.46	0.71	0.47	0.44	0.52	1.34
154								
159								
168 169								
170								
171	0.07	-5.82	0.94	0.85	0.63	0.44	0.33	0.10
175								
212								
225 230								
237								
238								
253								
256 273								
309								
311								
313								
323 333								
334								
336								
339								
342								
349 351								
356	-0.22	0.22	0.17	0.57	0.31	0.08	0.14	0.61
360	1.67	2.41	2.23	1.70	1.73	1.34		-0.42
370 372	-0.05	0.22	-0.22	-0.28	0.00	-0.82	0.33	0.61
381								
445	-0.95	-0.60	-1.11	-1.00	-0.61	-0.84	-0.98	-0.22
447 463	1.38	 1.58	3.01	4.25	4.89			-2.29
495								
507								
541								
551 558								
575								
610								
621 621								
631 633								
634								
657	-0.05	0.22	0.04	0.14	0.15	-0.28	-0.63	0.30
704	-0.45	-0.71	-0.48	-0.42	-0.48	-0.46	-0.63	0.20
732 752	-0.58 -0.45	-0.74 -0.09	0.16 0.04	-0.35 0.00	0.00 0.79	-0.18 0.26	0.08 -0.25	0.61 -0.22
753								
778								
781 785	-0.62	-1.34	-1.38	-0.85 0.43	-0.64 0.79	-0.10		-1.04
763 798	-0.05 	0.33	-0.35 	0.43	0.79	1.52		-0.01
823								
824								
825 840								
872	0.01	-0.51	-0.22	-0.85	-0.64	0.08		-0.53
873	-0.45	-0.61	-0.60	-0.42	-0.48	0.08		-0.63
874	-0.45	-0.71	-0.60	-0.28	-0.48	-0.10		-0.63
875	-0.27	-1.03	-0.60	0.00	-0.16	1.34		-0.42
887 902								
904								
913								
914 962								
962 963	-0.65	-0.49	-1.00	 -1.61	-1.68	-2.25		-0.17
971	0.59	0.35	-0.04	0.03	0.18	0.29	0.35	0.47
974								

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lab	IBP	5%rec	10%rec	20%rec	30%rec	40%rec	50%rec	FBP
994	0.24	0.12	-0.48	-0.14	0.47	1.34	1.10	1.24
995	0.24	-0.61	-0.67	-0.70	-0.56	-0.01	0.04	0.77
996								
997								
1011								
1016								
1026								
1040								
1065								
1108	0.65	-0.27	-0.23	0.85	0.50	-0.30	-0.21	0.66
1109								
1121								
1126								
1134								
1140								
1167								
1205								
1212								
1213								
1277								
1299								
1320	0.53	-1.55	-0.09	0.29	-0.48	-0.28	-0.06	0.20
1356								
1367								
1381								
1397								
1402	1.27	1.58	0.68	0.00	-0.16	-0.10	0.33	0.61
1510								
1556								
1585								
1586	-0.45	-0.46	-1.55	-0.39	-1.24	-1.24	-1.08	-0.66
1631								
1635								
1648								
1650								
1681								
1720								
1724								
1740								
1776			0.05			0.07	0.77	0.47
1792		0.20	0.35	0.34	-0.02	0.27	0.77	0.47
1796								
1854								
1857 1881	-0.27	0.00	0.00	-0.28	0.33	0.00	0.52	0.72
1906	-0.27	-0.09	-0.09 	-0.26	-0.32 	0.08	0.52	0.72
1900								
1986	-0.45	-0.19	-0.09	0.43	-0.16	-0.46	-0.25	0.30
2129	0.41	2.20	2.49	2.27	2.21	0.98	-0.25	0.50
6054	0.41	2.20	2.43	2.21				
6075								
6092								
6112	0.01	0.80	0.67	0.34	0.28	0.00	-0.42	-0.31
6114	-1.05	-1.28	-2.46	-1.38	-0.40	-1.04	-3.16	-1.67
6201	-0.49	0.19	1.17	5.44		0.36	3.30	2.82
6238								
6262								
6298								
6340								
6359								
			-	-	-	-	•	•

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Determination of Total Carbon, Hydrogen and Nitrogen on sample #20250; results in %M/M

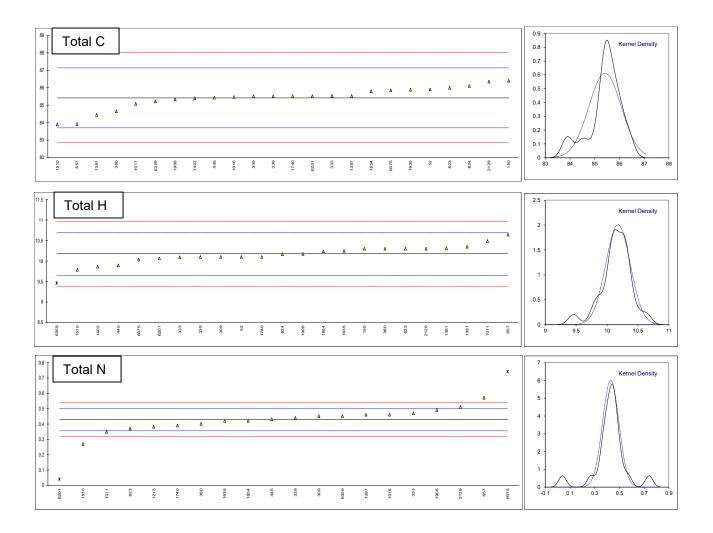
lab	method	Total C	mark	z(targ)	Total H	mark	z(targ)	Total N	mark	z(targ)
52		85.9		0.56	10.1		-0.29			
120 140										
150		86.4		1.14	10.3		0.47			
154										
159 168										
169										
170										
171 175										
212										
225										
230 237										
238										
253										
256										
273 309	D5291-C	85.5		0.09	10.1		-0.29	0.45		0.56
311	50201 0									
313										
323 333	D5291-A	85.52		0.12	10.09		-0.33	0.47		 1.11
334	D0201-A						-0.00			
336										
339 342		85.5		0.09	10.10		-0.29	0.44		0.29
342										
351										
356	DE004 A				40.00		0.47			
360 370	D5291-A	84.64		-0.91 	10.30		0.47	0.40		-0.81
372										
381	D=004.0									
445 447	D5291-C	85.43		0.01	9.89		-1.09 	0.43		0.01
463										
495										
507 541										
551										
558										
575										
610 621										
631										
633										
634 657	D5291-D	83.91		 -1.75	10.64		1.76	0.57	С	3.86
704	D3291-D			-1.75					C	3.00
732										
752 753										
753 778										
781										
785										
798 823	D5291-D	86.0		0.67	10.3		0.47	0.37		-1.64
824	D0201 D	86.09		0.78	10.16		-0.07			
825										
840 872										
873										
874										
875										
887 902										
904										
913										
914										
962 963										
971										
974										

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lab	method	Total C	mark	z(targ)	Total H	mark	z(targ)	Total N	mark	z(targ)
994										
995 996										
997										
1011		85.08		-0.40	10.48		1.15	0.35		-2.19
1016		85.46		0.05				0.461		0.87
1026										
1040 1065										
1108										
1109										
1121										
1126										
1134 1140										
1167										
1205										
1212	D=004.4									
1213 1277	D5291-A							0.381		-1.34
1277										
1320										
1356										
1367										
1381 1397	D5291-A	84.445 85.53		-1.13 0.13	10.306 10.35		0.49 0.66	0.46		0.84
1402	D3291-A	85.39		-0.04	9.86		-1.20	0.40		0.04
1510	D5291-D	83.89		-1.78	9.78		-1.51	0.27		-4.39
1556										
1585										
1586 1631										
1635	D5291-D	85.87		0.52	10.25		0.28	0.42		-0.26
1648	502015									
1650										
1681										
1720 1724										
1740	D5291-A	85.5		0.09	10.1		-0.29	0.39		-1.09
1776	2020.71									
1792										
1796	DE204 D	 0E 0		0.44	10.00		0.20	0.40		0.26
1854 1857	D5291-D	85.8		0.44	10.23		0.20	0.42		-0.26
1881										
1906		85.323	С	-0.11	10.168	С	-0.03	0.490	С	1.66
1949										
1986	DE201 A	86.35		1.08	10.30		0.47	0.51		2.21
2129 6054	D5291-A	60.33		1.00	10.30		0.47	0.51		2.21
6075	D5291-D	85.84		0.49	10.03		-0.56	0.74	C,R(0.01)	8.54
6092									, ,	
6112										
6114 6201	D5291-A	85.510		0.10	10.064		-0.43	0.0394	R(0.01)	 -10.74
6238	D3291-A						-0.43	0.0394	13(0.01)	-10.74
6262										
6298										
6340						D(0.05)		0.450		
6359		85.21		-0.24	9.459	R(0.05)	-2.72	0.450		0.56
normali	ity	OK			OK			suspect		
n	•	24			22			18		
outliers		0			1			2		
mean (ı		85.4203			10.1771			0.4296		
st.dev. R(calc.)		0.65160 1.8245			0.19855 0.5560			0.06627 0.1855		
	D5291-ABC:16)	0.86079			0.3360			0.1655		
	91-ABC:16)	2.4102			0.7382			0.1018		
,	,	•			•			•		Į

Lab 657 first reported 0.81 Lab 1906 first reported 83.36, 9.551, 0.545 Lab 6075 first reported 0.94

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Determination of Aluminum as Al, Silicon as Si and total Al+Si on sample #20251; results in mg/kg

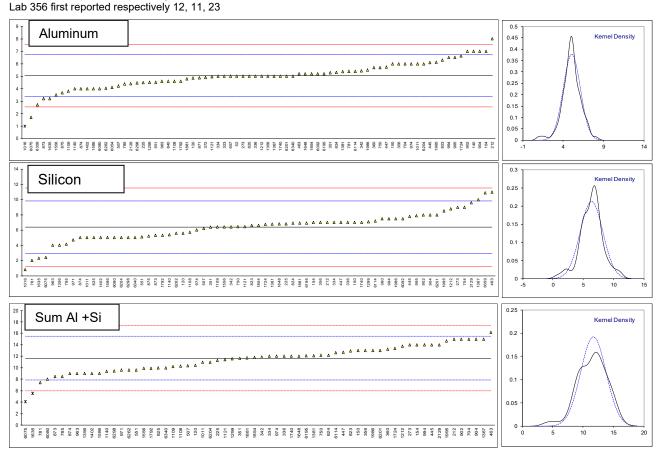
lab	method	Al	mark	z(targ)	Si	mark	z(targ)	Sum Al+Si	mark	z(targ)
52	IP501	5		-0.07	<10			<15		(****
120	IP501	4.8525		-0.25	5.583		-0.47	10.4355		-0.66
140	IP501	7		2.32	<10					
150	IP501	6	С	1.12	7		0.35	13	С	0.69
154	IP501	7	Ü	2.32	7		0.35	14	Ü	1.21
159		, 			, 					
169										
170										
171	IP501	<5			<10			<15		
175	11 301									
212	IP470	8		3.52	7		0.35	15		1.73
225	IP501	4.48		-0.70	6.83			11.31		
230	IP470		C		<10	C	0.25	<15	C	-0.20
	IP470	<5	С			С			С	
237	IDE04			0.07			4.50	4.4		4.04
273	IP501	5		-0.07	9		1.52	14		1.21
311	IP501	<5		0.07	<10			<15		
323	IP501	5		-0.07	<10			<15		
333	IP501	<5			<10			<15		
334	IP501	5		-0.07	7		0.35	12		0.16
336	IP501	5		-0.07	7		0.35	12		0.16
342	IP501	5.43327		0.45	6.4309		0.02	11.8636		0.09
351	IP501	5.28		0.26	6.39	_	0.00	11.67	_	-0.01
356	IP501	6	С	1.12	7	С	0.35	13	С	0.69
360	IP501	5.7		0.76	7.5		0.64	13.2		0.79
370	IP470	< 5			< 10			< 15		
372	IP470	4.9		-0.19	<10			<15		
381										
445	IP501	6.1		1.24	7.8		0.82	14		1.21
447	IP501	5.74		0.81	7.00		0.35	12.74		0.55
463	IP470	5.2		0.17	11.0		2.68	16.2		2.36
495										
507	IP501	4.2		-1.03	6.2		-0.11	10.4		-0.67
541	IP501	<5			<10			<15		
551	IP501	4.503		-0.67	5.125		-0.74	9.628		-1.08
631										
657	IP501	5		-0.07	<10			<15		
704	IP470	6		1.12	9		1.52	15		1.73
750	IP501	5.70		0.76	6.46		0.04	12.16		0.25
781	IP501	5.4		0.41	2.0		-2.56	7.4		-2.24
785	IP470	4.38		-0.82	4.14		-1.31	8.5		-1.67
798										
823	IP501	6.3		1.48	6.6		0.12	12.9		0.63
824	IP501	5.3		0.29	6.9		0.30	12.2		0.27
825	IP501	5		-0.07	5		-0.81	10		-0.88
840	D5184	4.6		-0.55	<10			<15		
872	20.0.									
873	IP470	3.2		-2.23	5.3		-0.64	8.5		-1.67
874	IP501	4		-1.27	5		-0.81	9		-1.41
875	IP501	3.68		-1.65	5.2		-0.69			
902	IP501	7		2.32	8		0.94	15		1.73
904	IP501	7		2.32	8		0.94	15		1.73
913	001	, 								
963	IP501	4.6		-0.55	4		-1.39	9		-1.41
971	IP501	4.87		-0.23	4.71		-0.98	9.58		-1.41
974	IP501	6		1.12	6		-0.23	12		0.16
994	IP501	6.5		1.72	7.5		0.64	14		1.21
995	IP470	6.5		1.72	7.87		0.86			
1011	ISO10478			1.12			-0.81	11		-0.36
		6 1	D(0.05)	-4.86	5 0.8		-3.26			-0.30
1016	In house		R(0.05)							
1040	ID470	4.0			 		0.40	40.0		0.70
1108	IP470	4.6		-0.55	5.7		-0.40	10.3		-0.73
1109	IP470	3.8		-1.51	6.4		0.00	10.2		-0.78
1121	IP501	4.97		-0.11	6.46		0.04	11.4		-0.15
1126										
1134	15504									
1140	IP501	3.992		-1.28	5.384		-0.59	9.376		-1.21
1212	IP501	5.0		-0.07	8.8		1.40	13.8		1.11
1213	IDE04									
1299	IP501	4.5		-0.67	7.1		0.41	11.6		-0.05
1356	ISO10478	5		-0.07	4		-1.39	9		-1.41
1367	IP501	5		-0.07	10		2.10	15		1.73
1381	ISO10478	5.36		0.36	6.77		0.22	12.13		0.23
1402	IP501	4		-1.27	5		-0.81	9		-1.41
1556	IP501	3.5		-1.87	6.4		0.00	9.9		-0.94

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lab	method	Al	mark z(targ)	Si	mark	z(targ)	Sum Al+Si	mark	z(targ)
1586	IP470	4	-1.27	5		-0.81	9		-1.41
1635	D5185	3.2	-2.23	2.3		-2.38	5.5	DG(0.05)	-3.24
1648	IP501	5.20	0.17	6.81		0.24	12.01	, ,	0.17
1720									
1724	IP501	6.627	1.87	6.757		0.21	13.384		0.89
1740	IP501	5	-0.07	7		0.35	12		0.16
1792	IP501	4.6	-0.55	5.3		-0.64	9.9		-0.94
1796									
1854	IP501	5.2	0.17	6.6		0.12	11.8		0.06
1857									
1881	IP470	4.8	-0.31	6.9		0.30	11.7		0.01
1949									
1986	IP470	5.5	0.53	7.5		0.64	13		0.69
1995	IP501	6.13	1.28	8.52		1.24	14.65		1.55
2129	IP470	4.4	-0.79	9.6		1.87	14.0		1.21
6054	IP501	4.10686	-1.14						
6075	In house	1.7	-4.02	2.4		-2.32	4.1	DG(0.05)	-3.97
6080	IP501	4.0	-1.27	5.0		-0.81	8.0	E ` ´	-1.93
6092	IP501	5.2	0.17	7.5		0.64			
6114	IP501	5.4	0.41	7.2		0.47	12.6		0.48
6195	IP501	5.2	0.17	6.9		0.30	12.1		0.22
6201	IP501	5	-0.07	8		0.94	13		0.69
6204	IP501	6.0	1.12	5.0		-0.81	11.0		-0.36
6262	IP501	4.03	-1.23	5.58		-0.47	9.61		-1.09
6298	IP501	4.46	-0.72	5.00		-0.81	9.46		-1.17
6340	IP501	5	-0.07	5		-0.81	10		-0.88
6359		2.7	-2.83	10.9		2.62			
	normality	suspect		suspect			OK		
	n	75		69			62		
	outliers	1		0			2		
	mean (n)	5.06		6.39			11.69		
	st.dev. (n)	1.058		1.877			2.082		
	R(calc.)	2.96		5.26			5.83		
	st.dev.(IP470:05)	0.835		1.718			1.910		
	R(IP470:05)	2.34		4.81			5.35		
compa	re								
	R(IP501:05)	1.71		2.12			2.72		

Lab 150 first reported respectively 8, 15 Lab 230 first reported respectively 0, 0, 0

Lab 6080: possibly calculation difference. lis calculated 9



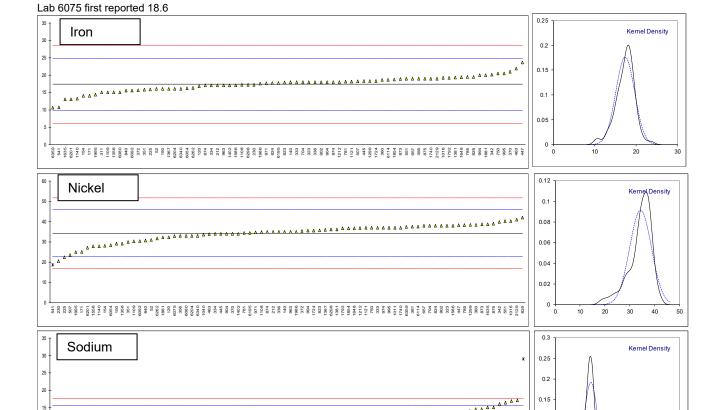
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Determination of Iron as Fe, Nickel as Ni, Sodium as Na on sample #20251; results in mg/kg

lab	method	Fe	mark	z(targ)	Ni	mark	z(targ)	Na	mark	z(targ)
52	IP501	16		-0.37	31		-0.57	11		-0.27
120	IP501	16.755		-0.17	32.225		-0.36	11.815		0.14
140	IP501	18		0.16	35		0.11	17		2.71
150	IP501	16		-0.37	29		-0.92	11		-0.27
154	IP501	14		-0.91	28		-1.09	13		0.73
159										
169										
170										
171	IP501	14		-0.91	25		-1.60	29	R(0.01)	8.65
175									, ,	
212	IP470	17		-0.10	35		0.11	14		1.22
225	IP501	15.87		-0.41	22.34		-2.06	9.09		-1.21
230	IP470	17.2295		-0.04	20.4782		-2.38	16.8932		2.65
237										
273										
311	IP501	15		-0.64				10		-0.76
323	IP501	18		0.16	38		0.63	12		0.23
333	IP501	18		0.16	37		0.46	11		-0.27
334	IP501	17		-0.10	34		-0.06	5		-3.24
336	IP501	18		0.16	35		0.11	13		0.73
342	IP501	20.1551		0.74	39.7945		0.94	10.2702		-0.63
351	IP501	15.78		-0.43	29.91		-0.76	11.82		0.14
356	IP501	19		0.43	33		-0.23	16		2.21
360	IP501	18.6		0.32	38.4		0.70	11.6		0.03
370	IP470	21		0.97	34		-0.06	12		0.23
372	IP470	15.6		-0.48	35.4		0.18	11.1		-0.22
381					37.5		0.54			
445	IP501	18.3		0.24	34.0		-0.06	16.4		2.41
447	IP501	23.65		1.67	38.16		0.66	12.01		0.24
463	IP470	21.9		1.21	33.8		-0.09	12.0		0.23
495										
507	IP501	18.2		0.22	23.5		-1.86	11.9		0.18
541	IP501	10.7		-1.79	18.6	R(0.05)	-2.70	9.0		-1.26
551	IP501	18.977		0.43	40.300		1.02	13.718		1.08
631										
657	IP501	19		0.43	38		0.63	13		0.73
704	IP470	18		0.16	38		0.63	12		0.23
750	IP501	20.48		0.83	36.99		0.46	12.33		0.39
781	IP501	18.1		0.19	34.3		-0.01	10.7		-0.41
785	IP470	19.49		0.56	38.28		0.68	13		0.73
798										
823	IP501	17.9		0.14	35.7		0.23	12.8		0.63
824	IP501	17.7		0.08	38.0		0.63	12.4		0.43
825	IP501	19.5		0.56	42		1.32	10		-0.76
840	IP501	15.5		-0.50	30.6		-0.64	10.4		-0.56
872	15.450									
873	IP470	18.9		0.40	38.7		0.75	12.0		0.23
874	IP501	17		-0.10	35		0.11	11		-0.27
875	IP501	19		0.43	39		0.80	12		0.23
902	IP501	18		0.16	38		0.63	10		-0.76
904	IP501	18		0.16	34		-0.06	10		-0.76
913	IDE01	17		0.10	25		0.11	15		1 72
963 071	IP501	17		-0.10 0.06	35 34.7		0.11	15		1.72
971 974	IP501 IP501	17.6 18		0.06 0.16	34.7 37		0.06 0.46	11.8 12		0.13 0.23
974 994	IP501	20		0.16	37 35.5			10.0		-0.76
995	IP470	20.5		0.70	37		0.20 0.46	12.1		0.28
1011	15470	20.5			37		0.46	9.4		-1.06
1011	In house	19.2			40.3		1.02	10.677		
1040	In house	19.2		0.48			-0.14	10.677		-0.43
1108	IP470	17.2		-0.05	33.53 34.8		0.08	8.8		-1.36
1109	IP470	15.0		-0.64	30.2		-0.71	11.2		-0.17
1121	IP501	18.1		0.19	36.9		0.44	11.1		-0.17 -0.22
1121	11 001	10.1		0.19						-0.22
1134										
1140	IP501	13.19		-1.12	27.82		-1.12	10.80		-0.36
1212	IP501	18.0		0.16	36.8		0.42	12.4		0.43
1213	501									
1299	IP501	18.3		0.24	38.3		0.68	11.4		-0.07
1356	IP501	15.5		-0.64	29		-0.92	11.4		-0.07
1367	IP501	16		-0.04	36		0.29	15		1.72
1381	D5863-A	19.28		0.51	36.15		0.23			1.72
1402	IP501	17		-0.10	34		-0.06	11		-0.27
1556	•••			-0.10	27.8		-1.12			0.68
		1			-			-		

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lab	method	Fe	mark z(targ)	Ni	mark	z(targ)	Na	mark	z(targ)
1586	IP470	17	-0.10	38		0.63	11		-0.27
1635	D5185	13.0	-1.17	38.7		0.75	5.94		- 2.77
1648	IP501	19.39	0.54	36.68		0.40	11.40		-0.07
1720									
1724	IP501	18.30	0.24	35.53		0.21	11.63		0.05
1740	IP501	19	0.43	37		0.46	11		-0.27
1792	IP501	19.2	0.48	36.6		0.39	12.6		0.53
1796									
1854	IP501	18.7	0.35	36.6		0.39	11.1		-0.22
1857									
1881	IP470	20.0	0.70	32.2		-0.37	9.5		-1.01
1949									
1986	IP470	17.5	0.03	35		0.11	10.5		-0.51
1995	IP501	14.36	-0.81	24.89		-1.62	14.54		1.49
2129	IP470	19.0	0.43	41		1.14	12		0.23
6054	IP501	16.2120	-0.31	28.3576		-1.03	9.91313		-0.80
6075				32.8		-0.26	8.63	С	-1.44
6080	IP501	15.0	-0.64	33.0		-0.23	8.0		-1.75
6092	IP501	15.5	-0.50	30.3		-0.69	13.8		1.12
6114	IP501	18.6	0.32	37.5		0.54	11.8		0.13
6195	IP501	17.7	0.08	34.4		0.01	9.4		-1.06
6201	IP501	13	-1.17	27		-1.26	11		-0.27
6204	IP501	16.0	-0.37	33.0		-0.23	11.0		-0.27
6262	IP501	16.31	-0.29	31.68		-0.46	9.91		-0.81
6298	IP501	17.22	-0.04	36.14		0.31	14.50		1.47
6340	IP501	16	-0.37	33		-0.23	11		-0.27
6359		10.6	-1.82	37.3		0.51	10.3		-0.61
	normality	suspect		suspect			suspect		
	n	78		81			79		
	outliers	0		1			1		
	mean (n)	17.39		34.33			11.54		
	st.dev. (n)	2.272		4.375			2.071		
	R(calc.)	6.36		12.25			5.80		
	st.dev.(IP470:05)	3.739		5.826			2.018		
	R(IP470:05)	10.47		16.31			5.65		
compa				1					
	R(IP501:05)	4.51		11.76			4.09		



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9.334 9.305 9.

0.05

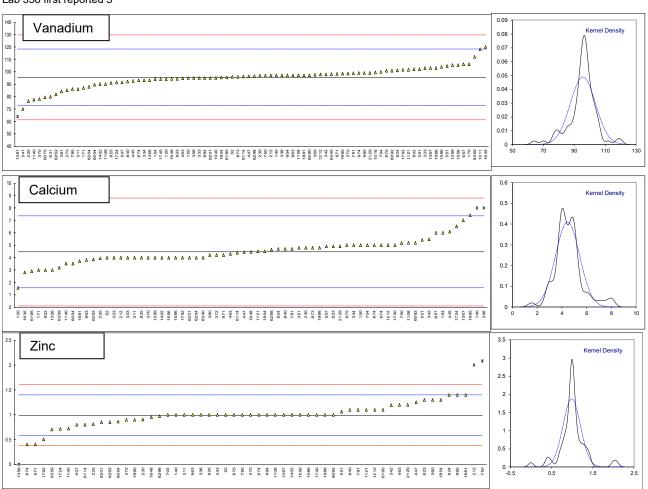
Determination of Vanadium as V, Calcium as Ca and Zinc as Zn on sample #20251; results in mg/kg

Section	lab	method	V	mark	z(targ)	Ca	mark	z(targ)	Zn	mark	z(targ)
140 P501 97	52		96			4					
150 P501 95 -0.05 5 0.37 51	120	IP501			-0.13	1.566					
150 P501 94	140	IP501	97		0.12	8	R(0.05)		1		0.04
159	150	IP501	95		-0.05	5	, ,		<1		
1868		IP501	94		-0.14	6		1.06	<1		
170											
171											
175 05863-8 106											
221						3		-1.01	<1		
1.00											
237										R(0.01)	
273 PS01								-0.36			
273		IP470									-0.44
311		ID-0.4									
323 IPS01 95 0.05 4 0.32 51 0.04 334 IPS01 95 0.05 4 0.32 51 0.04 334 IPS01 97 8619 0.12 54779 0.70 1.1909 0.97 355 IPS01 97 8619 0.20 54779 0.70 1.1909 0.97 356 IPS01 97 8619 0.20 54779 0.70 1.1909 0.97 357 IPS01 98 0.06 0.57 4.79 0.70 1.1909 0.97 358 IPS01 96 0.06 0.57 4.79 0.70 1.1909 0.97 358 IPS01 97 0.12 0.06 0.57 4.79 0.70 0.18 1.30 1.50 370 IPS01 98 0.06 0.26 0.26 0.26 0.18 1.30 1.50 370 IPS01 98 0.26 0.26 0.26 0.18 0.9 0.44 372 IP470 98 0.26 0.26 0.11 0.04 447 IPS01 96 0.88 0.08 4.43 0.02 1.25 1.26 463 IP470 94.7 0.08 4.3 0.011 1.2 1.01 445 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 351 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 351 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 351 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 352 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 353 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 354 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 355 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 356 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 357 IPS01 91.5 0.36 4.9 0.30 0.8 0.93 358 IPS01 91.5 0.36 0.37 0.11 0.60 359 IPS01 91.5 0.36 0.37 0.11 0.04 350 IPS01 92.2 0.30 0.15 0.60 0.33 351 IPS01 95.7 0.16 0.16 0.16 0.10 350 IPS01 95.7 0.16 0.16 0.16 0.10 350 IPS01 91.5 0.36 0.37 0.16 0.16 0.10 350 IPS01 91.5 0.36 0.37 0.17 0.16 0.14 350 IPS01 92.2 0.30 0.7 0.16 0.14 350 IPS01 92.2 0.30 0.7 0.16 0.14 0.32 351 IPS01 92.2 0.30 0.7 0.16 0.14 0.32 352 IPS01 91.0 0.40 0.40 0.32 0.40 0.40 352 IPS01 92.2 0.30 0.7 0.16 0.10 0.40 353 IPS01 95.0 0.05 0.05 0.07 0.10 0.40 350 IPS01 95.0 0.05 0.05 0.07											
333 P501 95 -0.05 4 -0.32 1 0.04 334 P501 97 0.12					-0.84						0.04
334 P501 93 0.23 5 0.37 <1 0.04 342 P501 978619 0.20 5.4779 0.70 1.1909 0.97 351 P501 95 0.05 8 R(0.05) 2.44 <1 C 0.04 356 P501 95 0.05 8 R(0.05) 2.44 <1 C 0.04 356 P501 97.6 0.18 4.2 0.18 1.3 0.150 370 P470 78 1.55 4 0.32 1 0.04 381 P501 84.1 1.01 0.04 447 P501 84.8 0.02 6.1 1.13 0.15 447 P501 95.6 0.26 6.1 1.13 0.04 448 P501 94.7 0.08 4.3 0.02 1.25 1.26 489 P470 94.7 0.08 4.3 0.01 1.2 0.01 489 P501 91.5 0.36 4.9 0.30 0.8 0.93 481 P501 91.5 0.36 0.91 0.65 0.65 41 P501 0.16 0.16 0.11 0.64 481 P501 0.16 0.16 0.17 0.04 482 P501 0.16 0.16 0.17 0.04 483 P470 94.7 0.00 0.33 0.65 0.37 1 0.04 484 P501 0.66 0.91 0.66 0.91 0.66 0.91 0.66 0.91 485 P501 0.69 0.93 0.8 0.37 1 0.04 486 P501 0.69 0.69 0.84 0.08 4.1 0.04 487 P501 0.69 0.00 0.33 0.8 0.37 1 0.04 488 P501 0.69 0.60 0.03 4.8 0.23 1 0.04 489 P501 0.60 0.00 0.34 4.9 0.30 1.3 1.50 484 P501 0.60 0.60 0.60 0.60 0.60 0.60 484 P501 0.60 0.60 0.60 0.60 0.60 0.60 484 P501 0.60 0.60 0.60 0.60 0.60 0.60 0.60 484 P501 0.60 0.60 0.60 0.60 0.60 0.60 0.60 0.60 485 P501 0.60 0											0.04
336					-0.05	4					0.04
342 P501 97.8619 0.20 5.4779 0.70 1.1909 0.97 356 P501 95 0.05 8 R(0.05) 2.44 <1 C 356 P501 97.6 0.18 4.2 -0.18 1.3 1.50 370 P470 78 -1.55 4 -0.32 1 0.04 381 P501 84.1 -1.01 381 P501 84.1 -1.01 381 P501 94.7 98.6 0.26 4.2 -0.18 0.9 -0.44 381 P501 84.1 -1.01 381 P501 94.8 0.08 4.43 -0.02 1.25 1.26 381 P501 94.8 0.08 4.43 -0.02 1.25 1.26 381 P501 95.6 0.26 0.26 6.1 1.13 -1 381 P501 95.6 0.26 0.26 6.1 0.11 1.2 1.01 382 P501 95.7 0.36 4.9 0.30 0.8 0.93 383 P470 94.7 0.08 4.3 -0.01 1.2 1.00 384 P501 70.1 2.24 3 381 P501 70.1 0.35 0.36 4.9 0.30 0.8 0.93 381 P501 70.1 0.25 0.36 4.9 0.30 0.8 0.93 381 P501 70.1 0.25 0.36 0.66 1.060 0.33 381 P501 94.7 0.00 0.31 0.66 1.060 0.33 381 P501 95.0 0.997 0.12 0.16 0.04 381 P501 98.7 0.27 4.7 0.16 0.48 2.08 R(0.01) 5.29 382 P501 94.3 0.11 4.9 0.30 1.3 1.50 383 P501 94.3 0.11 0.48 4.7 0.16 1.1 0.53 384 P501 94.3 0.11 0.44 4 0.32 1 0.04 384 P501 94.3 0.11 0.48 4.7 0.16 1.1 0.53 387 P501 94.3 0.11 0.44 0.23 1 0.04 381 P501 95.0 0.00 0.00 4.8 0.23 0.37 1 0.04 381 P501 95.0 0.00 0.00 0.00 0.00 0.00 384 P501 97 0.12 0.56 0.37 1 0.04 384 P501 98.2 0.30 4.7 0.16 1.1 0.53 387 P501 98.2 0.30 4.7 0.16 1.1 0.53 387 P501 98.2 0.30 0.30 0.37 1 0.04 381 P501 99 0.30 0.30 0.37 1 0.04 381 P501 99 0.30 0.30 0.37 1 0.04 381 P501 99 0.30 0.30 0.37 1 0.04 381 P501											0.04
356 P501 950 0.057 4.79 0.22 <1 360 P501 97.6 0.05 8 R(0.05) 2.44 <1 C 360 P501 97.6 0.18 4.2 0.18 1.3 1.50 370 P470 98.6 0.26 4.2 0.18 0.9 0.04 372 P470 98.6 0.26 4.2 0.18 0.9 0.04 445 P501 92.6 0.26 6.1 1.13 <1 445 P501 92.6 0.26 6.1 1.13 <1 447 P501 96.48 0.08 4.43 0.02 1.25 1.26 463 P470 94.7 0.08 4.3 0.011 1.2 1.01 475 P501 91.5 0.36 4.9 0.30 0.8 0.93 541 P501 91.5 0.36 4.9 0.30 0.8 0.93 541 P501 70.1 2.24 <3 1.1 551 P501 104 635 0.79 5.418 0.66 1.060 0.33 657 P501 106 0.91 6 1.06 <1 657 P501 106 0.91 6 1.06 <1 657 P501 99.87 0.12 5.16 0.48 2.08 R(0.01) 5.29 785 P470 86 0.84 1.1 0.04 786 P501 99.3 0.11 4.9 0.30 1.3 1.50 823 P501 91 0.40 4 0.32 1 0.04 824 P501 91 0.40 4 0.32 1 0.04 825 P501 91 0.04 4 0.32 1 0.04 826 P501 91 0.04 4 0.32 1 0.04 827 P501 99 0.30 4.8 0.23 1 0.04 828 P501 91 0.04 4 0.32 1 0.04 829 P501 92 0.30 4.8 0.23 1 0.04 824 P501 91 0.40 4 0.32 1 0.04 825 P501 91 0.04 4 0.32 1 0.04 826 P501 91 0.04 4 0.32 1 0.04 827 P501 99 0.30 5 0.37 1 0.04 828 P501 91 0.2 0.56 0.33 1.1 0.53 837 P470 99 0.30 5 0.37 1 0.04 840 P501 93 0.00 0.33 4.8 0.23 1 0.04 841 P501 93 0.00 0.33 4.8 0.23 1 0.04 842 P501 91 0.00 0.03 4.8 0.23 1 0.04 843 P501 99 0.30 0.00 0.00 0.00 0.00 844 P501 99 0.30 0.00 0.00 0.00 0.00 0.00 850 P501 99 0.30 0.00											
356 P501 95 0.05 8 R(0.05) 2.44 <1 C					0.20						0.97
360 P501 97.6 0.18 4.2 0.18 1.3 1.50 370 P470 98.6 0.26 4.2 0.18 0.9 0.04 372 P470 98.6 0.26 4.2 0.18 0.9 0.04 381 P501 92.6 0.26 6.1 1.13 <1					-0.57		P(0.05)			C	
370							11(0.00)			C	1 50
372 P470											
381 P501 84.1					0.26						
445 P501 92.6 0.26 6.1 1.13 <1											
443 P501 96.48 0.08 4.43 -0.02 1.25 1.26											
A63 P470 94.7 0.08 4.3 0.11 1.2 1.01											1.26
A95									1.2		
551 IP501 70.1 -2.24 <3											
551 IP501 104.635 0.79 5.418 0.66 1.060 0.33 631 DS863-A 80.001 -1.37	507	IP501	91.5		-0.36	4.9		0.30	0.8		-0.93
631 DS863-A 80.001 -1.37	541	IP501	70.1		-2.24	<3			<1		
667 IP501 106 0.91 6 1.06 <1	551		104.635		0.79	5.418		0.66	1.060		0.33
TOA											
750 19501 96.97											
781 IP501 98.7 0.27 4.7 0.16 1.1 0.53 785 IP470 86 -0.84 1 0.04 823 IP501 94.3 -0.11 4.9 0.30 1.3 1.50 824 IP501 101.1 0.48 4.7 0.16 1.4 1.99 825 IP501 91 -0.40 4 -0.32 1 0.04 840 IP501 92.2 -0.30 4.7 0.16 1.1 0.53 872 873 IP470 96.0 0.03 4.8 0.23 874 IP501 93 -0.23 5 0.37 0.4 -2.287 875 IP501 101 0.47 5 0.37 1 0.04 902 IP501 97 0.12 <1											
785 IP470 86 -0.84 <										R(0.01)	
Region R											
823 IP501 94.3 -0.11 4.9 0.30 1.3 1.50 824 IP501 101.1 0.48 4.7 0.16 1.4 1.99 825 IP501 91 -0.40 4 -0.32 1 0.04 840 IP501 92.2 -0.30 4.7 0.16 1.1 0.53 872		IP470									0.04
824 IP501 101.1 0.48 4.7 0.16 1.4 1.99 825 IP501 91 -0.40 4 -0.32 1 0.04 840 IP501 92.2 -0.30 4.7 0.16 1.1 0.53 872		IDE04									4.50
825 IP501 91 -0.40 4 -0.32 1 0.04 840 IP501 92.2 -0.30 4.7 0.16 1.1 0.53 872											1.50
840 IP501 92.2 -0.30 4.7 0.16 1.1 0.53 872 IP470 96.0 0.03 4.8 0.23			-								
872											
873 IP470 96.0 0.03 4.8 0.23		11 30 1									
874 IP501 93 -0.23 5 0.37 0.4 -2.87 875 IP501 101 0.47 5 0.37 1 0.04 902 IP501 102 0.56 3 -1.01 <1		IP470									
875 IP501 101 0.47 5 0.37 1 0.04 902 IP501 102 0.56 3 -1.01 <1					-0.23						-2 87
902 IP501 97						5					
904 IP501 97 0.12 <1 913 963 IP501 97 0.12 3.8 -0.46 1 0.04 971 IP501 98.2 0.23 4.2 -0.18 0.4 -2.87 974 IP501 99 0.30 5 0.37 1 0.04 994 IP501 95 -0.05 1 0.04 995 IP470 99 0.30 1.4 1.99 1011 D5863-B 118 1.97 1.4 1.99 1014 IP501 95.01 -0.05 1.4 1.99 1016 In house 99.5 0.34 1.0 1108 D5863-B 97.0 0.12 5.2 0.51 1.0 0.04 1109 IP470 90.1 -0.48 1.0 11121 IP501 101.6 0.53 4.5 0.02 1.1 0.53 1126 1134 1140 IP501 97.8 0.19 5.0 0.37 1.1 0.53 1213 1129 IP501 103 0.65 7 1.75 1 0.04 1381 D5863-A 63.97 R(0.05) -2.78 1402 IP501 90 -0.49 4 -0.32 1.0 0.04 1556 IP501 90 -0.49 4 -0.32 1.0 0.04 1556 IP501 90 -0.49 4 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 90 -0.49 4 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04					0.56						
913 963 IP501 97 0.12 3.8 -0.46 1 0.04 971 IP501 98.2 0.23 4.2 -0.18 0.4 -2.87 974 IP501 99 0.30 5 0.37 1 0.04 994 IP501 95 -0.05 1 101 D5863-B 118 1.97 1016 In house 99.5 0.34 1040 IP501 95.01 95.01 -0.05 1108 D5863-B 97.0 0.12 5.2 0.51 1.0 0.04 1199 1121 IP501 101.6 0.53 1126 1134 1134 1134 1134 1134 1134 1134 1134 11356 IP501 105.4 0.86 4.0 0.86 4.0 0.86 4.0 0.04 105.4 0.04 105.4 0.04 105.4 0.06 1 0.04 10.04	904								<1		
963 IP501 97 0.12 3.8 -0.46 1 0.04 971 IP501 98.2 0.23 4.2 -0.18 0.4 -2.87 974 IP501 99 0.30 5 0.37 1 0.04 994 IP501 95 -0.05 1 1 0.04 995 IP470 99 0.30 1.4 1.99 1011 D5863-B 118 1.97 1.016 In house 99.5 0.34 1.016 In house 99.5 0.34 1.016 IP501 95.01 -0.05 1.040 IP501 90.1 -0.05 1.040 IP501 101.6 0.53 4.5 0.02 1.1 0.53 1126 1.140 IP501 101.6 0.53 4.5 0.02 1.1 0.53 1126 1.140 IP501 77.65 -1.58 3.509 -0.66 0.723 -1.30 1213 1.30 1213 1.30 1213 1.30 1256 IP501 103 0.65 7 1.75 1 0.04 1381 D5863-A 63.97 R(0.05) -2.78 1.49 1.054 0.86 4.0 -0.32 1.0 0.04 1556 IP501 90 0.49 4 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 0.86 4.0 -0.32 1.0 0.04 1556 IP501 105.4 0.86 4.0 0.86 4.0 0.032 1.0 0.04 1556 IP501 105.4 0.86 4.0 0.06 105.4 0.06											
974 IP501 99 0.30 5 0.37 1 0.04 994 IP501 95 -0.05 1 0.04 995 IP470 99 0.30 1.4 1.99 1011 D5863-B 118 1.97 1.4 1.99 1016 In house 99.5 0.34 1040 IP501 95.01 -0.05 1108 D5863-B 97.0 0.12 5.2 0.51 1.0 0.04 1109 IP470 90.1 -0.48 1126 1134 1134 IP501 77.65 -1.58 3.509 -0.66 0.723 -1.30											
994 IP501 95 -0.05 1 0.04 995 IP470 99 0.30 1.4 1.99 1011 D5863-B 118 1.97											
995 IP470 99 0.30 1.4 1.99 1011 D5863-B 118 1.97						5		0.37			
1011 D5863-B 118 1.97											
1016 In house 99.5 0.34											1.99
1040 IP501 95.01 -0.05											
1108 D5863-B 97.0 0.12 5.2 0.51 1.0 0.04 1109 IP470 90.1 -0.48											
1109 IP470 90.1 -0.48											0.04
1121 IP501 101.6 0.53 4.5 0.02 1.1 0.53 1126 1134 1140 IP501 77.65 -1.58 3.509 -0.66 0.723 -1.30 1212 IP501 97.8 0.19 5.0 0.37 1.1 0.53 1213 1299 IP501 105.4 0.86 4.0 -0.32 <1.0											0.04
1126											0.53
1134		001									
1140 IP501 77.65 -1.58 3.509 -0.66 0.723 -1.30 1212 IP501 97.8 0.19 5.0 0.37 1.1 0.53 1213 1299 IP501 105.4 0.86 4.0 -0.32 <1.0											
1212 IP501 97.8 0.19 5.0 0.37 1.1 0.53 1213 1299 IP501 105.4 0.86 4.0 -0.32 <1.0		IP501									-1.30
1213 1											
1299 IP501 105.4 0.86 4.0 -0.32 <1.0											
1356 IP501 93 -0.23 3 -1.01 0 R(0.01) -4.82 1367 IP501 103 0.65 7 1.75 1 0.04 1381 D5863-A 63.97 R(0.05) -2.78 1402 IP501 90 -0.49 4 -0.32 1 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04	1299	IP501									
1367 IP501 103 0.65 7 1.75 1 0.04 1381 D5863-A 63.97 R(0.05) -2.78 1 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1 0.04 0.04	1356		93		-0.23	3				R(0.01)	-4.82
1381 D5863-A 63.97 R(0.05) -2.78 10.04 1402 IP501 90 -0.49 4 -0.32 1 0.04 1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04	1367	IP501			0.65	7			1	. ,	
1556 IP501 105.4 0.86 4.0 -0.32 1.0 0.04				R(0.05)							
1586 IP470 104 0.74 4 -0.32 1 0.04											
	1586	IP4/U	104		0.74	4		-0.32	1		0.04

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lab	method	V	mark z(tar		mark	z(targ)	Zn	mark	z(targ)
1635	D5185	120	2.	-	2	-1.13	<1		
1648	IP501	94.17	-0.	3 4.4	5	-0.01	0.95		-0.20
1720									
1724	IP501	91.43	-0.3		05	1.41	0.717		-1.33
1740	IP501	94	-0.			0.37	1		0.04
1792	IP501	101.5	0.9	2 4.0		-0.32	0.5		-2.39
1796					-				
1854	IP501	95.4	-0.0	2 4.5		0.02	1.3		1.50
1857	.= .=-								
1881	IP470	97.0	0.			-0.53	1.4		1.99
1949	ID 170				-				
1986	IP470	103	0.0		•	0.23	1		0.04
1995	IP501	98.45	0.2			2.04	0.9		-0.44
2129	IP470	99	0.3			0.30	1.2		1.01
6054	IP501	89.5393	-0.9		2161	-0.65	0.861337		-0.63
6075	D5863-B	79.5	-1.4		-				
6080	IP501	97.0	0.				<1		
6092	IP501	101	0.4			0.51	1.0		0.04
6114	IP501	96.2	0.0			-0.04	0.8		-0.93
6195	IP501	95.4	-0.0			-1.08	1.1		0.53
6201	IP501	95	-0.0			-0.32	0.85		-0.69
6204	IP501 IP501	88.0 81.81	-0.0 -1.2	-	E	-0.32 -0.42	<1.0		-0.69
6262 6298	IP501	96.48	-1 0.0			-0.42 0.14	0.85 0.97		
6340	IP501 IP501	98	0.0		0	-0.32	<1		-0.10
6359	1501	112.0	1.4			-0.32 -0.87	0.7		-1.42
0339		112.0	1.4	.4 3.2		-0.67	0.7		-1.42
	normality	suspect		2112	pect		suspect		
	n	85		67	poor		54		
	outliers	1		2			3		
	mean (n)	95.60		4.4	ĥ		0.99		
	st.dev. (n)	8.159		0.9			0.213		
	R(calc.)	22.84		2.7			0.60		
	st.dev.(IP470:05)	11.384		1.4			0.206		
	R(IP470:05)	31.88		4.0			0.58		
compai	. ,				-				
•	R(IP501:05)	25.92		1.7	0		0.51		

Lab 356 first reported 5



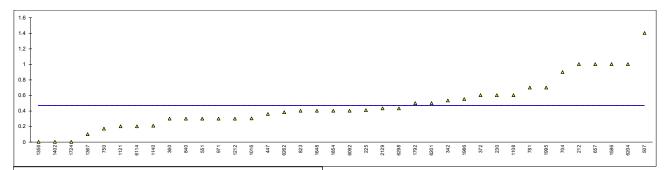
page 86 of 97 Fuel Oil: iis20F03

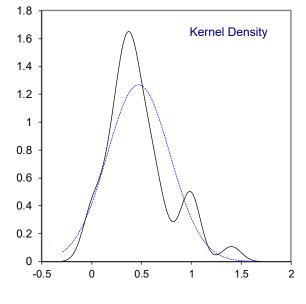
Determination of Phosphorus as P on sample #20251; results in mg/kg

Section Sect	lab	method	value	mark	z(targ)	remarks
				will		
156 159 169 170 171 171 175						
159						
169		IP501	<1			
171	159					
175	169					
175						
175		IP501	<1			
121 1250	175					
P501	212	IP500				
230 P601 0.6	225					
273 311 P501	220					
273 1501 <1	230	IF 30 I				
311	237					
1		IDE04				
333 P501	311					
334 P501	323					
336 PS01	333					
342 P501	334	IP501	<1			
351 PS01	336	IP501	<1			
351 PS01			0.5345			
356 PS01	351					
380 IPSO1				C		first reported 4
372 P500	360			· ·		mat reported.
381	370	11 00 1				
381	370	IDEOO				
447 F501	204	1500				
463 463 ————————————————————————————————	381	IDE04				
463						
495		IP501	0.36			
507 P501	463					
541 IP501 0.300	495					
551 IP501	507		1.4			
551 IP501	541	IP501	<1			
637 P501			0.300			
657 P501	631					
760	657	IP501				
750 P501 0.17	704					
785						
785 798 823 IP501 824 IP501 825 IP501 840 IP501 840 IP501 873 874 875 902 IP501 913 903 IP501 913 963 IP501 974 IP501 995 974 IP501 910 1011 1016 NEN6966 0.304 1109 1108 IP501 0.6 1109 11101 11108 IP501 0.6 11109 1121 IP501 0.2 1126 1134 1150 11501 0.3 11501 0.6 1170 1170 1170 1170 1170 1170 1170 117						
798 824 IP501 0.4 824 IP501 <1		IF 30 I				
823 P501						
824 IP501	798	15504				
825 IP501						
840 P501	824					
872 873 874 875 902 IP501 < 913 963 IP501 < 971 IP501 0.3 974 IP501 < 994 IP501 < 1011 1016 NEN6966 0.304 1108 IP501 0.6 1109 1121 IP501 0.2 1134 1134 1134 1134 11356 IP501 0.3 1367 IP501 0.1 1381 1381 1556	825					
873 874 875	840	IP501	0.3			
874 875	872					
874 875	873					
875	874					
902 P501						
904	902	IP501	<1			
913		001				
963						
971		IDEO1				
974						
994						
995 1011 1016 NEN6966						
1011 1016 NEN6966 0.304 1040 1108 IP501 0.6 1121 IP501 0.2 1134 1140 IP501 0.209 1212 IP501 0.3 1213 1219 1356 IP501 0.1 1381 1402 IP501 0 0 1556		IP501				
1016 NEN6966 0.304 1040 1108 IP501 0.6 1109 1121 IP501 0.2 1134 1140 IP501 0.209 1212 IP501 0.3 1213 1356 IP501 0 0 1367 IP501 0.1 1381 1402 IP501 0						
1040						
1040	1016	NEN6966	0.304			
1108 IP501 0.6 1109 1121 IP501 0.2 1126 1134 1140 IP501 0.209 1212 IP501 0.3 1299 1366 IP501 0 1381 1402 IP501 0 1556						
1109	1108	IP501				
1121 IP501 0.2 1126 1134 1140 IP501 0.209 1212 IP501 0.3 1213 1299 1356 IP501 0 1381 1402 IP501 0 1556		- = -				
1126 1134 1140 IP501 0.209 1212 IP501 0.3 1213 1299 1366 IP501 0 1381 1402 IP501 0 1556	1121	IP501				
1134		501				
1140 IP501 0.209 1212 IP501 0.3 1213 1299 1366 IP501 0 1381 1402 IP501 0 1556	1120					
1212 IP501 0.3 1213 1299 1356 IP501 0 1367 IP501 0.1 1381 1402 IP501 0 1556		IDEO4				
1213						
1299		IP501				
1356 IP501 0 1367 IP501 0.1 1381 1402 IP501 0 1556						
1367 IP501 0.1 1381 1402 IP501 0 1556						
1381 1402 IP501 0 1556						
1381 1402 IP501 0 1556	1367	IP501	0.1			
1402 IP501 0 1556	1381					
1556		IP501	0			
	1556	-				
		IP501	1			
	. 555	•.	•			

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lab	method	value	mark	z(targ)	remarks
1635	D5185	<1			
1648	IP501	0.40			
1720					
1724	IP501	0.00			
1740	IP501	<1			
1792	IP501	0.5			
1796					
1854	IP501	0.4			
1857					
1881					
1949					
1986	IP500	0.55			
1995	IP501	0.7			
2129	IP500	0.43			
6054					
6075					
6080	IP501	<1			
6092	IP501	0.4			
6114	IP501	0.2			
6195	IP501	<1			
6201	IP501	0.5			
6204	IP501	1.0			
6262	IP501	0.38			
6298	IP501	0.43			
6340	IP501	<1			
6359					
	n	63			
	mean (n)	<1			
	•				



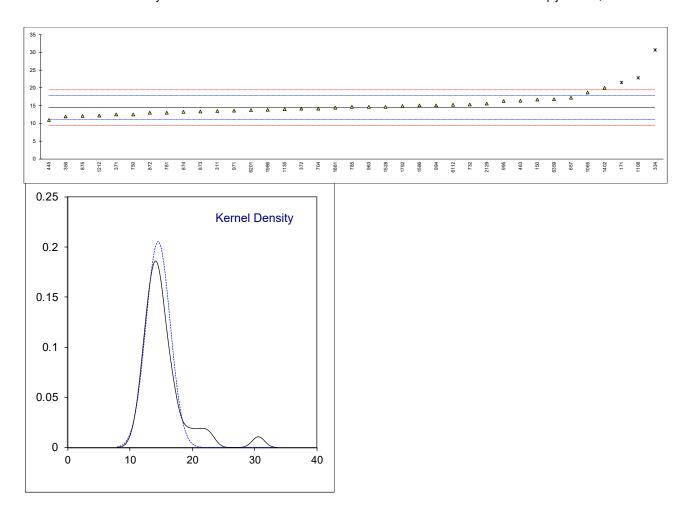


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Determination of Bromine Number on distillate <360°C AET on sample #20252; results in g Br₂/100g

lah	mothod	value	mark	z(tora)	romarke
lab	method D1150	value	шагк	z(targ)	remarks Describly false pagetive test result
120 140	D1159	<1.0 		<-8.07 	Possibly false negative test result
150	D1159	16.7		1.33	
170	200				
171	D1159	21.5	R(0.05)	4.20	
311	D1159	13.5		-0.59	
323					
334	D1159	30.6	R(0.01)	9.65	
356	D1159	11.9		-1.55	
371 372	D1159 D1159	12.48 14.1		-1.20 -0.23	
445	D1159	10.9		-0.23 -2.15	
463	D1159	16.39		1.14	
551					
657	D1159	17.2		1.63	
704	D1159	14.1		-0.23	
732	D1159	15.32		0.50	
750 750	D1159	12.5		-1.19	
752 781	D1159	13.0		-0.89	
785	D1159	14.6		0.07	
798	B 1 100				
823					
872	D1159	13.0		-0.89	
873	D1159	13.3		-0.71	
874	D1159	13.2		-0.77	
875 963	D1159 D1159	12.1 14.60	С	-1.43 0.07	First reported 23.42
971	D1159	13.53	C	-0.57	riist reported 25.42
994	D1159	15.02		0.32	
995	D1159	16.25		1.06	
1011					
1026					
1065	D1159	18.63	D(0.05)	2.48	
1108 1134	D1159	22.8	R(0.05)	4.98 	
1134	D1159	14.0		-0.29	
1212	D1159	12.16		-1.39	
1299					
1320					
1402	D1159	20		3.30	
1528	D1159	14.63		0.09	
1585 1586	D1159	15.0		0.31	
1792	D1159	14.888		0.24	
1857	21.00				
1862					
1881	D1159	14.39		-0.06	
1949					
1950 1986	D1159	13.8		 -0.41	
2129	D1159	15.5		0.61	
6112	D1159	15.2		0.43	
6201	D1159	13.71		-0.46	
6262					
6359	D1159	16.8		1.39	
	normality	OK			
	n	34			
	outliers	3			
	mean (n)	14.482			
	st.dev. (n)	1.9425			
	R(calc.)	5.439			
	st.dev.(D1159:07)	1.6699 4.676			
	R(D1159:07)	4.070			

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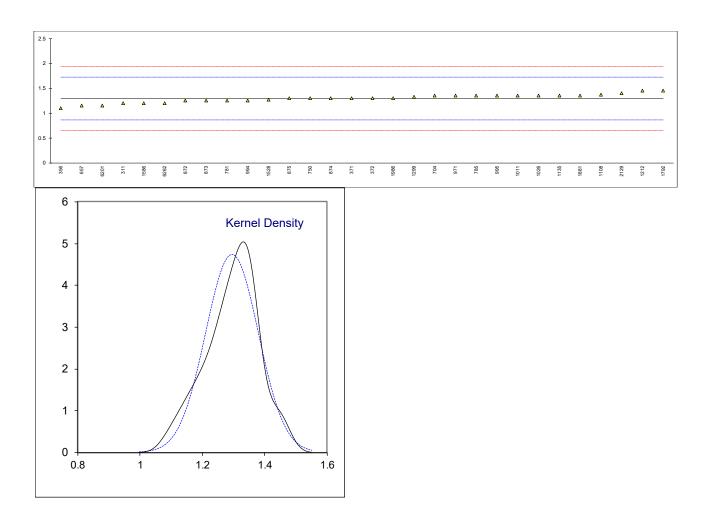


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Determination of P-Value on sample #20252

lab	method	value	mark	z(tara)	remarks
120	metriou		IIIdIK	z(targ)	Telliaiks
140					
150					
170					
171					
311	SMS1600	1.20		-0.45	
323					
334	0110100				
356	SMS1600	1.10		-0.91	
371 372	SMS1600	1.30		0.02	
445	SMS1600	1.30		0.02	
463					
551					
657	SMS1600	1.15		-0.68	
704	SMS1600	1.35		0.25	
732					
750	SMS1600	1.30		0.02	
752	01404000	4.05			
781	SMS1600	1.25		-0.21	
785 798	SMS1600	1.35 		0.25	
823					
872	SMS1600	1.25		-0.21	
873	SMS1600	1.25		-0.21	
874	SMS1600	1.30		0.02	
875	SMS1600	1.30		0.02	
963					
971	SMS1600	1.35		0.25	
994	SMS1600	1.25		-0.21	
995 1011	SMS1600 SMS1600	1.35 1.35		0.25 0.25	
1026	D7060	1.35		0.25	
1065	D1000				
1108	SMS1600	1.37		0.35	
1134					
1135	SMS1600	1.35		0.25	
1212	SMS1600	1.45		0.72	
1299	SMS1600	1.33		0.16	
1320					
1402 1528	D7112	1.27	С	-0.12	First reported 2.07
1585	DITTE		O	-0.12	That reported 2.07
1586	SMS1600	1.2		-0.45	
1792	SMS1600	1.45		0.72	
1857					
1862					
1881	SMS1600	1.35		0.25	
1949					
1950 1986	SMS1600	1.30		0.02	
2129	SMS1600	1.40		0.02	
6112	55.1000				
6201	SMS1600	1.15		-0.68	
6262	SMS1600	1.20		-0.45	
6359					
	***	014			
	normality	OK			
	n outliers	30 0			
	mean (n)	0 1.296			
	st.dev. (n)	0.0843			
	R(calc.)	0.236			
	st.dev.(SMS1600)	0.2143			
	R(SMS1600)	0.6			
	•				

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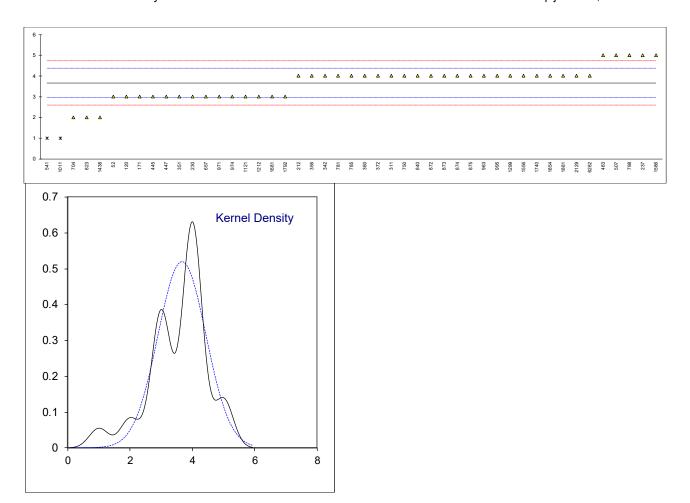


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Determination of Compatibility rating on sample #20253;

lab	method	value	mark	z(targ)		Ratio/remarks
52	D4740 Manual	3	IIIai K	-1.87	Original card	A+B=25g+30g
120	D4740 Manual	3		-1.87		A1D-20g100g
140	D4740 Mandai			-1.07		
154						
170						
171	D4740 Manual	3		-1.87		
212	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	
225						
228						
230	D4740 Manual	3		-1.87	Acc. to Reference Spot Description (Table 1)	
237	D4740 Manual	5		3.73	Copy of the original card	
311	D4740 Manual	4		0.93		A+B=12.5g+17.5g
323						
342	D4740 Manual	4		0.93	Copy of the original card	A+B=20.71+29.00g
351	D4740 Manual	3		-1.87	Original card	
356	D4740 Manual	4		0.93	Original card	A+B=24.90+34.90g
360	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	
372	D4740 Manual	4		0.93	Original card	
445	D4740 Manual	3		-1.87	Acc. to Reference Spot Description (Table 1)	
447	D4740 Manual	3		-1.87		
463	D4740 Manual	5		3.73	Acc. to Reference Spot Description (Table 1)	A+B=25+27g
507	D4740 Manual	5		3.73	Original card	
541	D4740 Manual	1	DG(0.05)	-7.47	Original card	
551					Acc. to Reference Spot Description (Table 1)	
657	D4740 Manual	3		-1.87	Original card	
704	D4740 Manual	2		-4.67	Acc. to Reference Spot Description (Table 1)	A+B=25+35g
750	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	
752	5.1-10.11					
781	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	A+B=20+28g
785	D4740 Manual	4		0.93	Copy of the original card	A+B=20+28g
798	D4740 Manual	5		3.73	 Original sand	
823	D4740 Manual	2		-4.67	Original card	
840	D4740 Manual	4		0.93	Copy of the original card	
872 873	D4740 Manual	4		0.93 0.93	Acc. to Reference Spot Description (Table 1)	
874	D4740 Manual	4 4		0.93	Ass. to Poference Shot Description (Table 1)	
875	D4740 Manual D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	
963	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	
971	D4740 Manual	3		-1.87		
974	D4740 Manual	3		-1.87	Original card	
995	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	A+B=25+28g
1011	D4740 Manual	1	DG(0.05)	-7.47	Acc. to Reference Spot Description (Table 1)	/ 2 _0 _0g
1065	2		20(0.00)		(azio :)	
1121	D4740 Manual	3		-1.87	Original card	A+B=25+30.5g
1134						= =9
1212	D4740 Manual	3		-1.87	Acc. to Reference Spot Description (Table 1)	
1299	D4740 Manual	4		0.93		
1438	D4740 Automated	2		-4.67		A+B=25+30.2g
1556	D4740 Manual	4		0.93	Copy of the original card	-
1585						
1586	D4740 Manual	5		3.73	Acc. to Reference Spot Description (Table 1)	
1681	D4740 Manual	3		-1.87	Acc. to Reference Spot Description (Table 1)	A+B=20+28g
1740	D4740 Manual	4		0.93	Acc. to Reference Spot Description (Table 1)	A+B=20+28g
1792	D4740 Manual	3		-1.87	Acc. to Reference Spot Description (Table 1)	A+B=25+29g
1854	D4740 Manual	4		0.93		
1881	D4740 Manual	4		0.93		
2129	D4740 Manual	4	_	0.93	Copy of the original card	
6262	D4740 Manual	4	С	0.93		First reported 1
	normality	OK				
	n	45				
	outliers	2				
	mean (n)	3.7				
	st.dev. (n)	0.77				
	R(calc.)	2.2				
	st.dev.(D4740-M:20)	0.36				
	R(D4740-M:20)	1				

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APPENDIX 2 Analytical details of the determination: Total Acid Number

lab	End point determination	Volume solvent	lab	End point determination	Volume solvent
52	Inflection Point	125 mL	904	Inflection Point	125 mL
120	Buffer End Point pH 10	125 mL	913		
140			914		
150			962		
154 159			963 971	Inflection Point	60 mL
168			971	Inflection Point	 125 mL
169			994	Inflection Point	125 mL
170	Inflection Point	60 mL	995	Inflection Point	125 mL
171	Inflection Point	60 mL	996		
175			997		
212	Inflection Point	125 mL	1011		
225			1016		
230			1026	Buffer End Point pH 10	125 mL
237 238			1040 1065	Inflection Point	60 mL
253			1108	Inflection Point	125 mL
256			1100	Inflection Point	125 mL
273			1121	Inflection Point	125 mL
309	Buffer End Point pH 11	60 mL	1126		
311	· ·		1134		
313			1140	Inflection Point	125 mL
323	Inflection Point	60 mL	1167		
336		405	1205	 B # 5 B : 1 11 10	405 1
333	Inflection Point	125 mL	1212	Buffer End Point pH 10	125 mL
334 339	Inflection Point	125 mL 	1213 1277		
342	Buffer End Point pH 11	125 mL	1299		
349		125 IIIL	1320		
351			1356		
356	Inflection Point	125 mL	1367		
360	Inflection Point	60 mL	1381		
370			1397		
372	Inflection Point	60 mL	1402	Buffer End Point pH 11	60 mL
381 445		 60 mL	1510 1556	 Buffer End Point pH 10	 125 mL
445	Inflection Point	125 mL	1585	Builer End Point ph 10	125 IIIL
463	Buffer End Point pH 11	125 mL	1586	Inflection Point	125 mL
495			1631		
507	Inflection Point	60 mL	1635		
541			1648	Buffer End Point pH 10	60 mL
551			1650		
558			1681		
575 610			1720 1724		
621			1724	Inflection Point	60 mL
631			1776		
633	Inflection Point	125 mL	1792	Inflection Point	60 mL
634			1796		
657	Inflection Point	125 mL	1854	Inflection Point	125 mL
704	Inflection Point	125 mL	1857		405 1
732	Inflaction Delict	 105 ml	1881	Inflection Point	125 mL
752 753	Inflection Point	125 mL	1906		
753 778			1949 1986	Inflection Point	 60 mL
781	Inflection Point	125 mL	2129	Inflection Point	125 mL
785			6054		
798			6075		
823	Inflection Point	125 mL	6092		
824	Inflection Point	125 mL	6112		
825			6114	Inflection Point	125 mL
840	Inflection Point	60 mL	6201	Inflection Point	125 mL
872	Inflection Point	125 mL	6238		
873 874	Buffer End Point pH 10 Buffer End Point pH 10	125 mL 125 mL	6262 6298	Inflection Point	 125 mL
875		125 IIIL 	6340	Inflection Point	125 mL
887			6359	Inflection Point	60 mL
902	Inflection Point	125 mL			
			•		

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APPENDIX 3

Number of participants per country

1 lab in ARGENTINA

1 lab in AUSTRALIA

1 lab in AZERBAIJAN

4 labs in BELGIUM

2 labs in BRAZIL

1 lab in BULGARIA

1 lab in CANADA

1 lab in COLOMBIA

1 lab in CONGO-BRAZZAVILLE

2 labs in COTE D'IVOIRE

2 labs in CROATIA

1 lab in DENMARK

1 lab in DJIBOUTI

1 lab in EGYPT

2 labs in ESTONIA

4 labs in FRANCE

2 labs in GEORGIA

2 labs in GERMANY

6 labs in GREECE 2 labs in INDIA

1 lab in INDONESIA

2 labs in ISRAEL

1 lab in KAZAKHSTAN

1 lab in LATVIA

2 labs in LITHUANIA

1 lab in MACEDONIA

1 lab in MALAYSIA

2 labs in MALTA

1 lab in MARTINIQUE

1 lab in MAURITIUS

1 lab in MOROCCO

7 labs in NETHERLANDS

2 labs in NIGERIA

1 lab in PANAMA

3 labs in PHILIPPINES

1 lab in POLAND

3 labs in PORTUGAL

1 lab in ROMANIA

17 labs in RUSSIAN FEDERATION

2 labs in SAUDI ARABIA

1 lab in SERBIA

1 lab in SINGAPORE

1 lab in SLOVAKIA

1 lab in SOUTH AFRICA

3 labs in SOUTH KOREA

5 labs in SPAIN

1 lab in SUDAN

4 labs in SWEDEN

1 lab in TAIWAN

1 lab in TANZANIA 1 lab in TOGO

5 labs in TURKEY

1 lab in TURKMENISTAN

2 labs in UKRAINE

7 labs in UNITED ARAB EMIRATES

10 labs in UNITED KINGDOM

10 labs in UNITED STATES OF AMERICA

2 labs in VIETNAM

1 lab in ZAMBIA

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APPENDIX 4

Abbreviations

C = final test result after checking of first reported suspect test result

 $\begin{array}{ll} D(0.01) &= \text{outlier in Dixon's outlier test} \\ D(0.05) &= \text{straggler in Dixon's outlier test} \\ G(0.01) &= \text{outlier in Grubbs' outlier test} \\ G(0.05) &= \text{straggler in Grubbs' outlier test} \\ DG(0.01) &= \text{outlier in Double Grubbs' outlier test} \\ DG(0.05) &= \text{straggler in Double Grubbs' outlier test} \\ \end{array}$

R(0.01) = outlier in Rosner's outlier test R(0.05) = straggler in Rosner's outlier test

E = calculation difference between reported test result and result calculated by iis

W = test result withdrawn on request of participant ex = test result excluded from statistical evaluation

n.a. = not applicable
n.e. = not evaluated
n.d. = not detected
fr. = first reported

SDS = Safety Data Sheet

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